

5G Electronics: Bridging the Measurement Challenges

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iNEMI orchestrated an industrial round robin

10 labs measuring identical samples with 4 different methods

- Split-cylinder resonators
- Split-post dielectric resonators
- Fabry Perot open resonators
- Balanced-type circular disk resonators

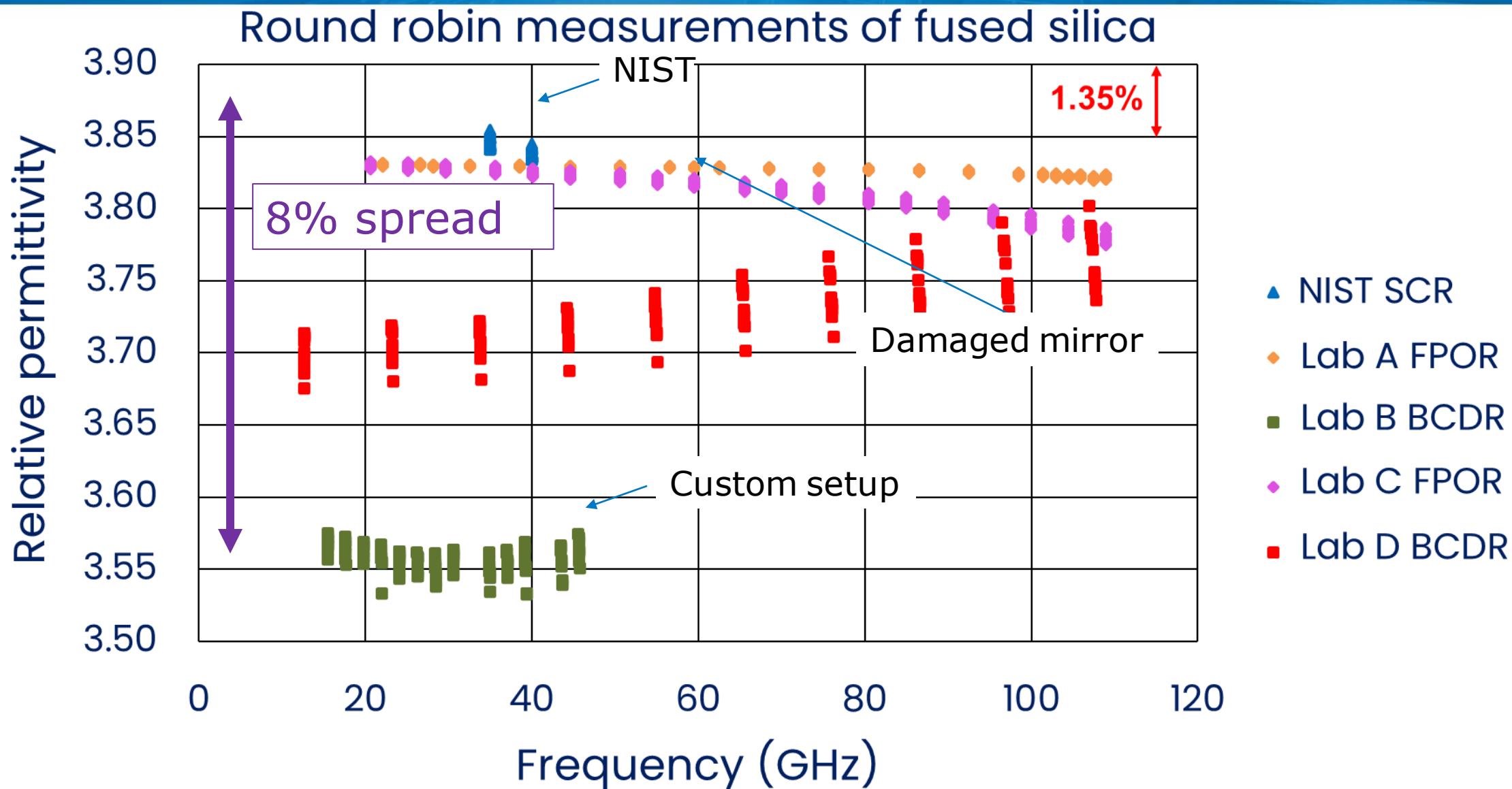


2 The results revealed a serious measurement problem

000242

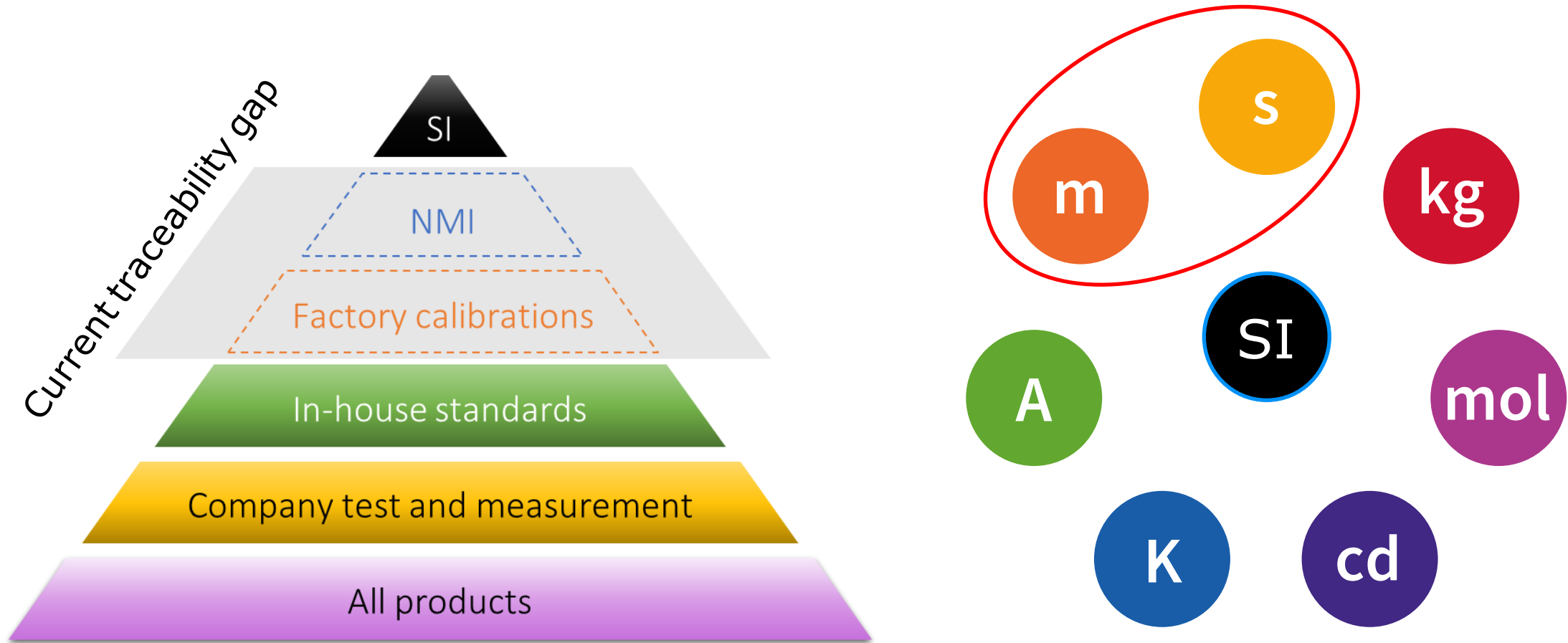


The semiconductor industry needs dielectric standards



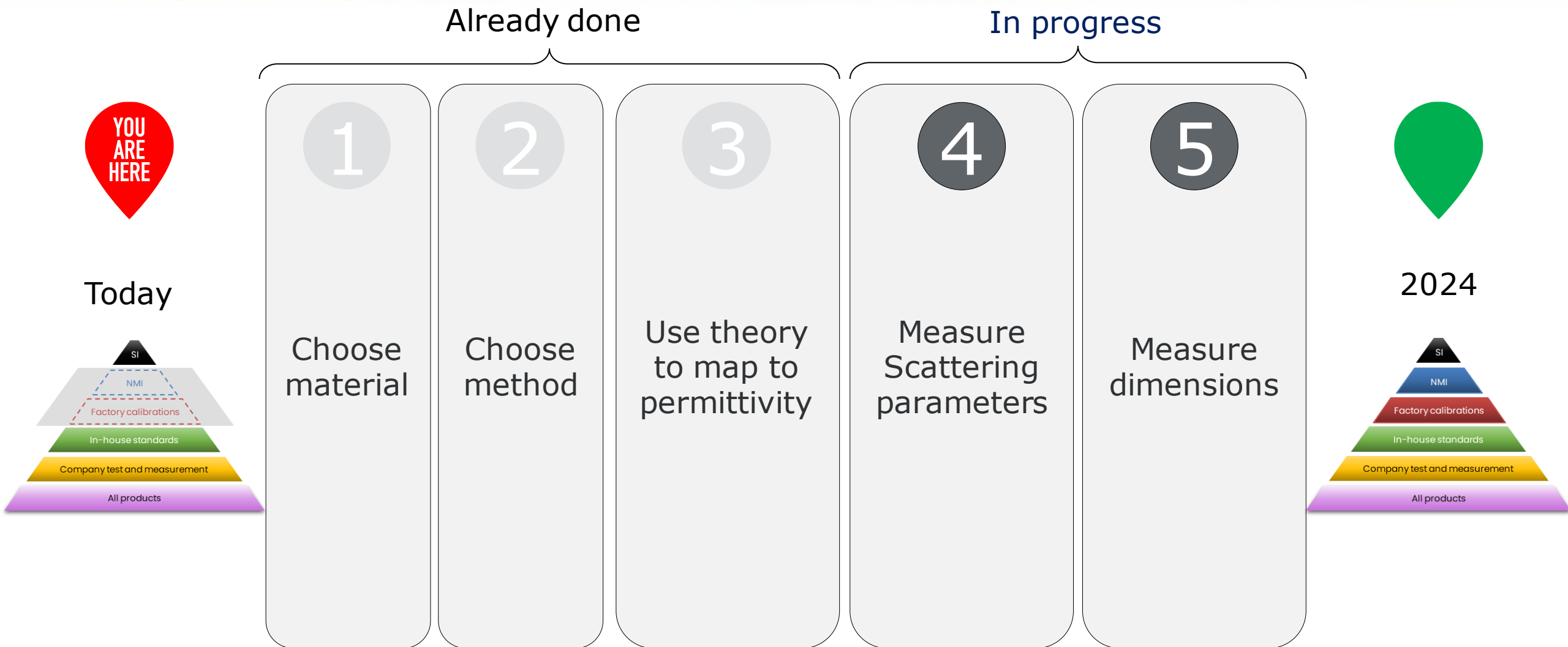
We need a traceable standard to know which answer is 'right'

Currently, there is no traceable standard



“Traceability” is an unbroken chain of measurements that end at the SI

We need to fill the traceability gap



Don't worry we are going to break down all these steps

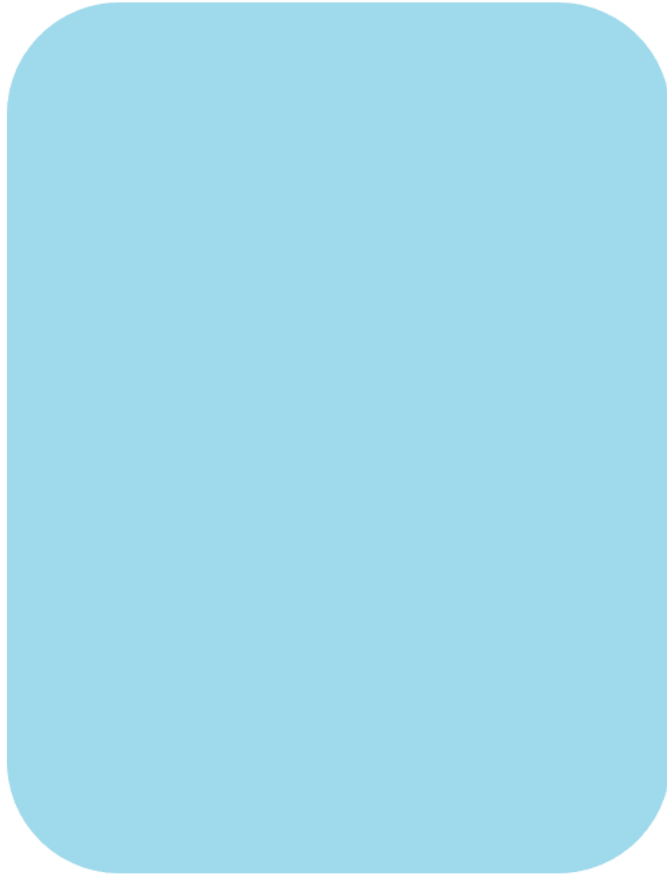
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We built a fused silica prototype to meet industry needs

1

Choose material

45 mm



35 mm

$$\epsilon' \approx 3.8$$
$$\tan \delta < 1e-3$$



150 μm $\pm$ **0.1 μm**

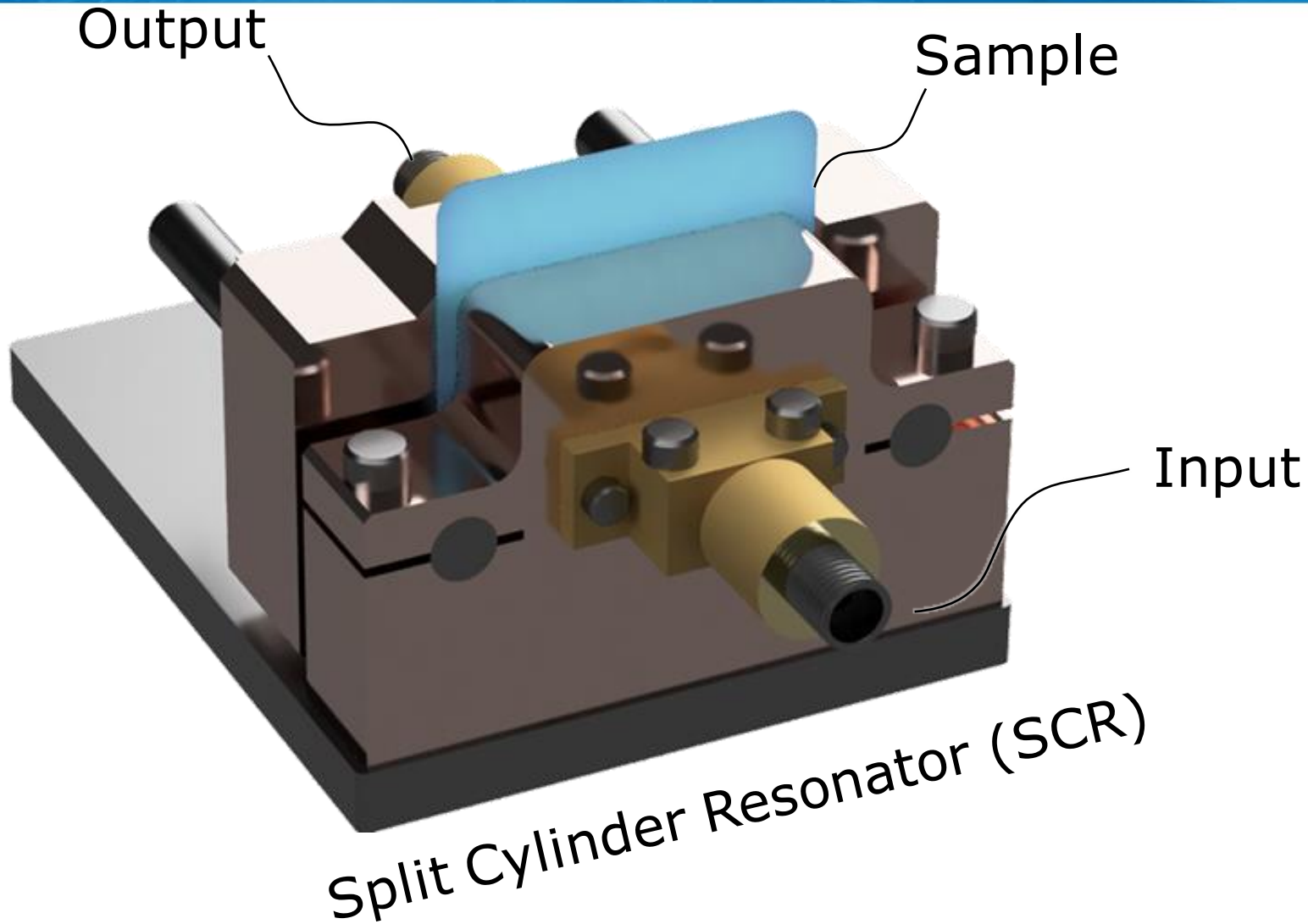
0.06% thickness variation

Thin + low ϵ' = compatible with commercially available resonators **INEMI**

We are using SCRs for this traceability path

2

Choose
method

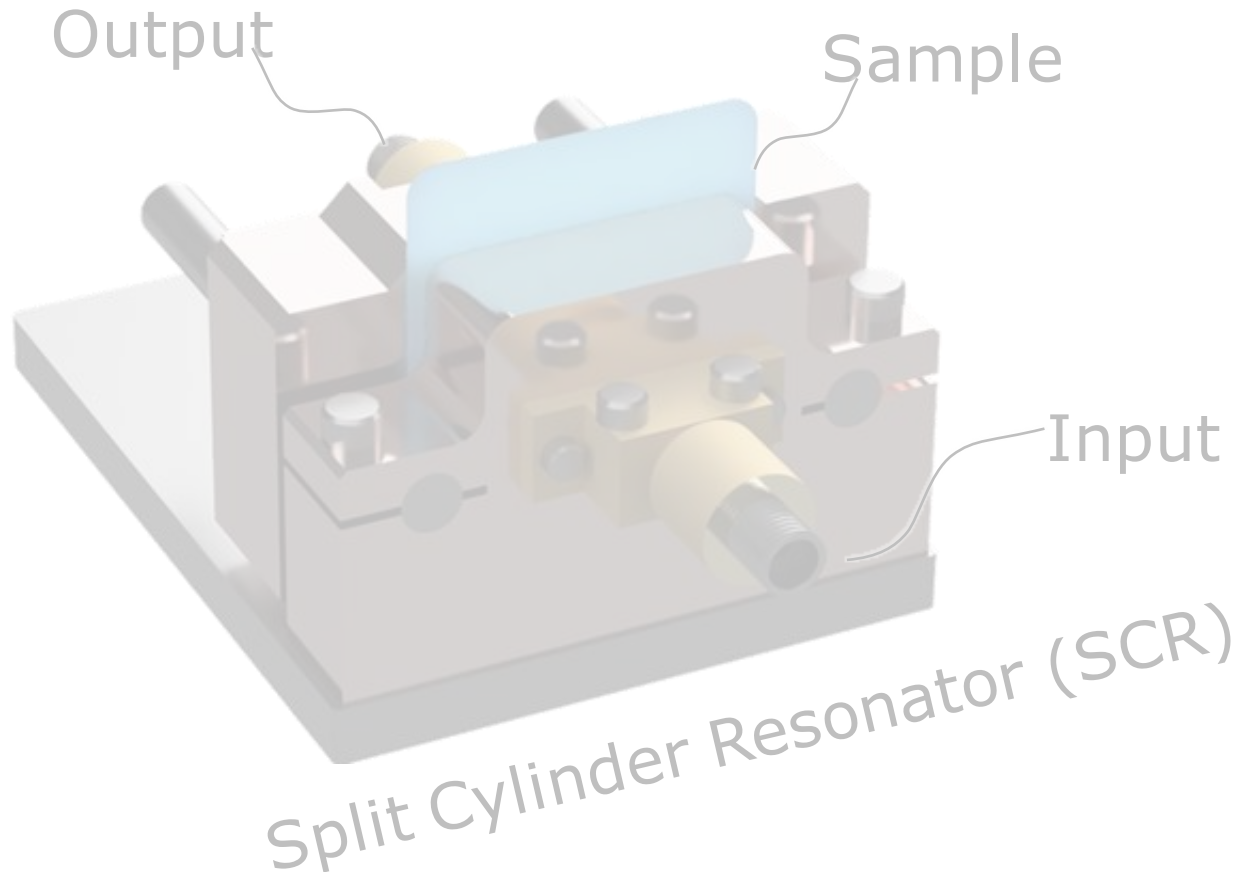


The dimensions of the cavity and sample are the critical features

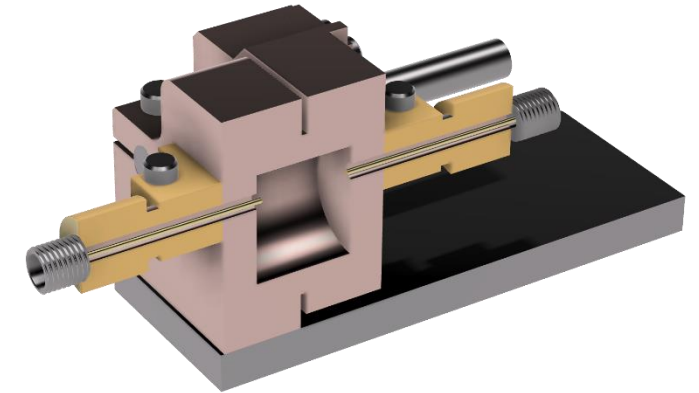
We are using SCRs for this traceability path

2

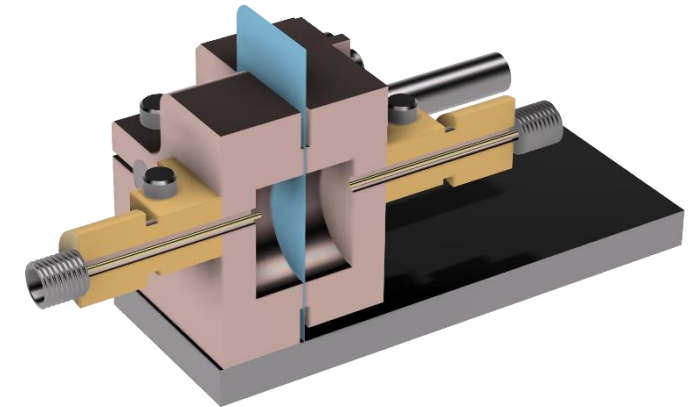
Choose
method



no sample



sample

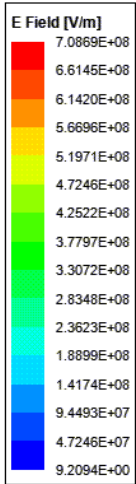


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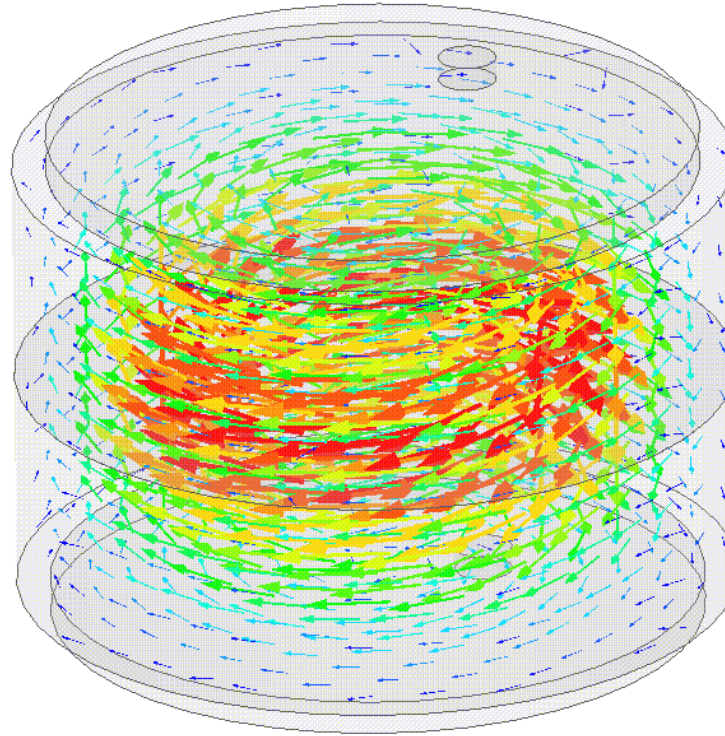
We know what the TE_{011} mode looks like

2

Choose
method



Phase = 0deg

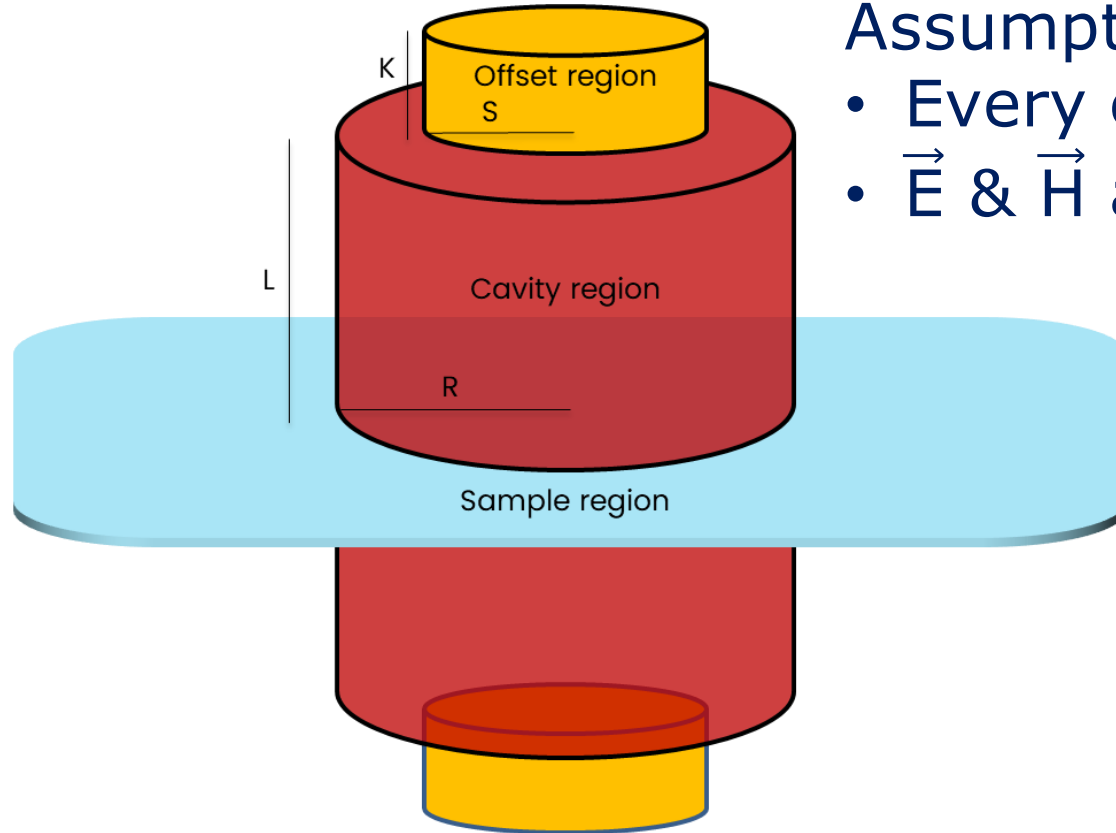


We use this mode's (perturbed) resonance frequency to
extract sample permittivity

We use mode-matching to extract permittivity

3

Use theory
to map to
permittivity



Assumptions:

- Every edge is a perfect conductor
- $\vec{E}$ & $\vec{H}$ are continuous at each interface

Analytical theory

Traceable dimensions + resonance frequency

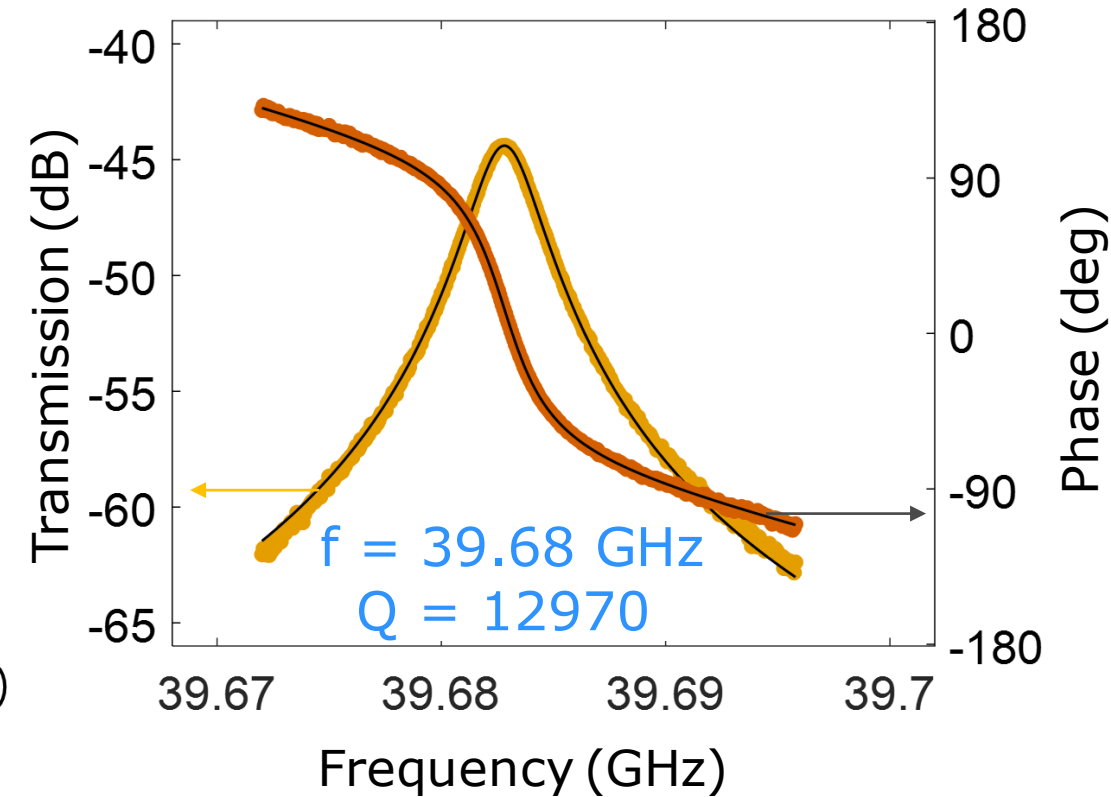
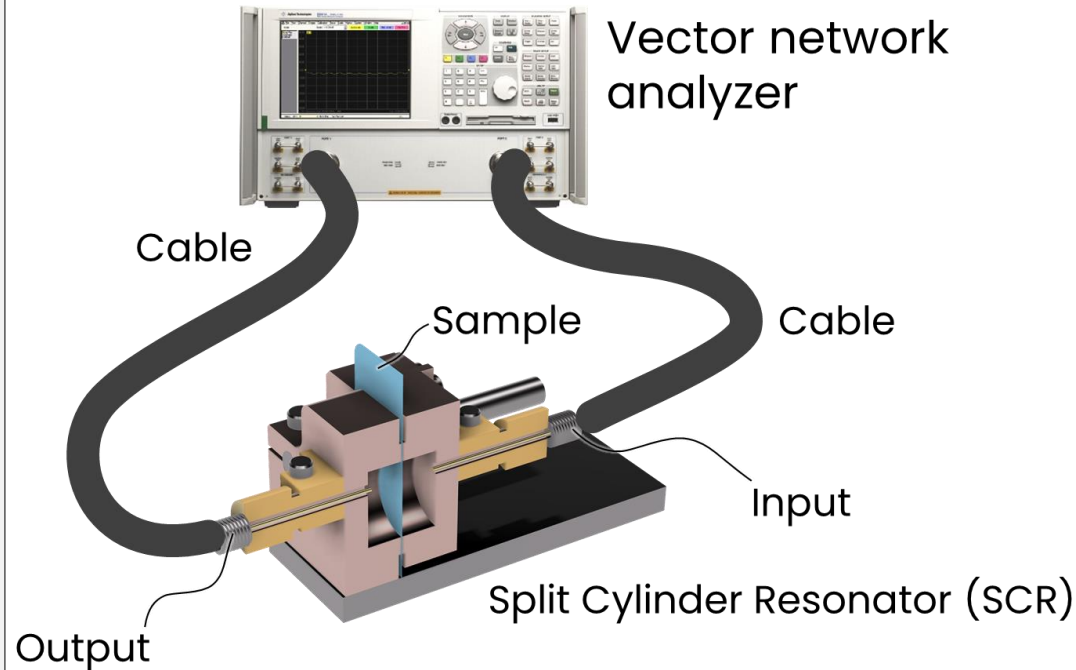


Traceable permittivity

We use a vector network analyzer (VNA) to measure f_{res} & Q

4

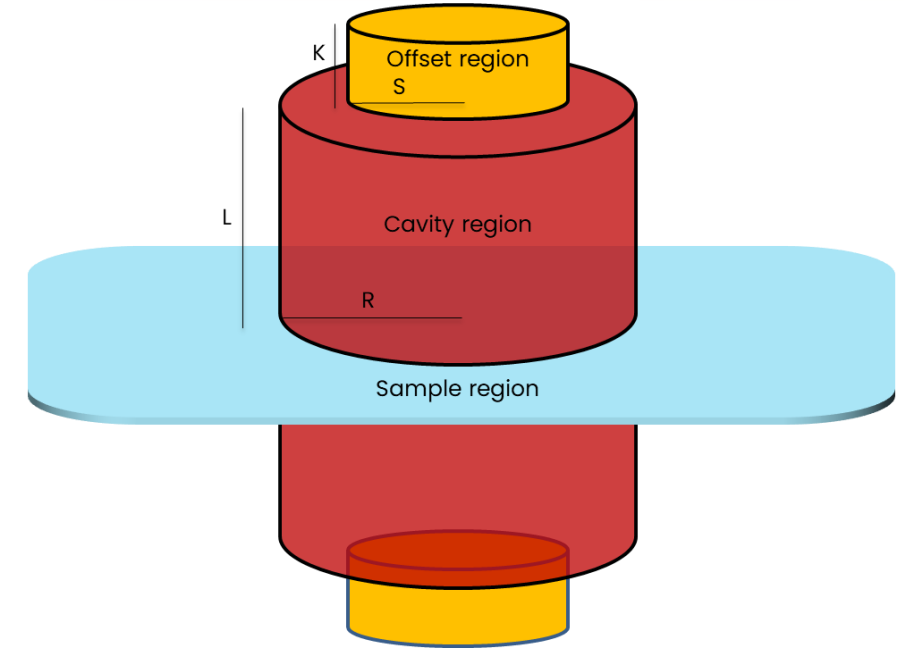
Measure
Scattering
parameters



NIST collaborators are dimensioning the cavities

5

Measure
dimensions



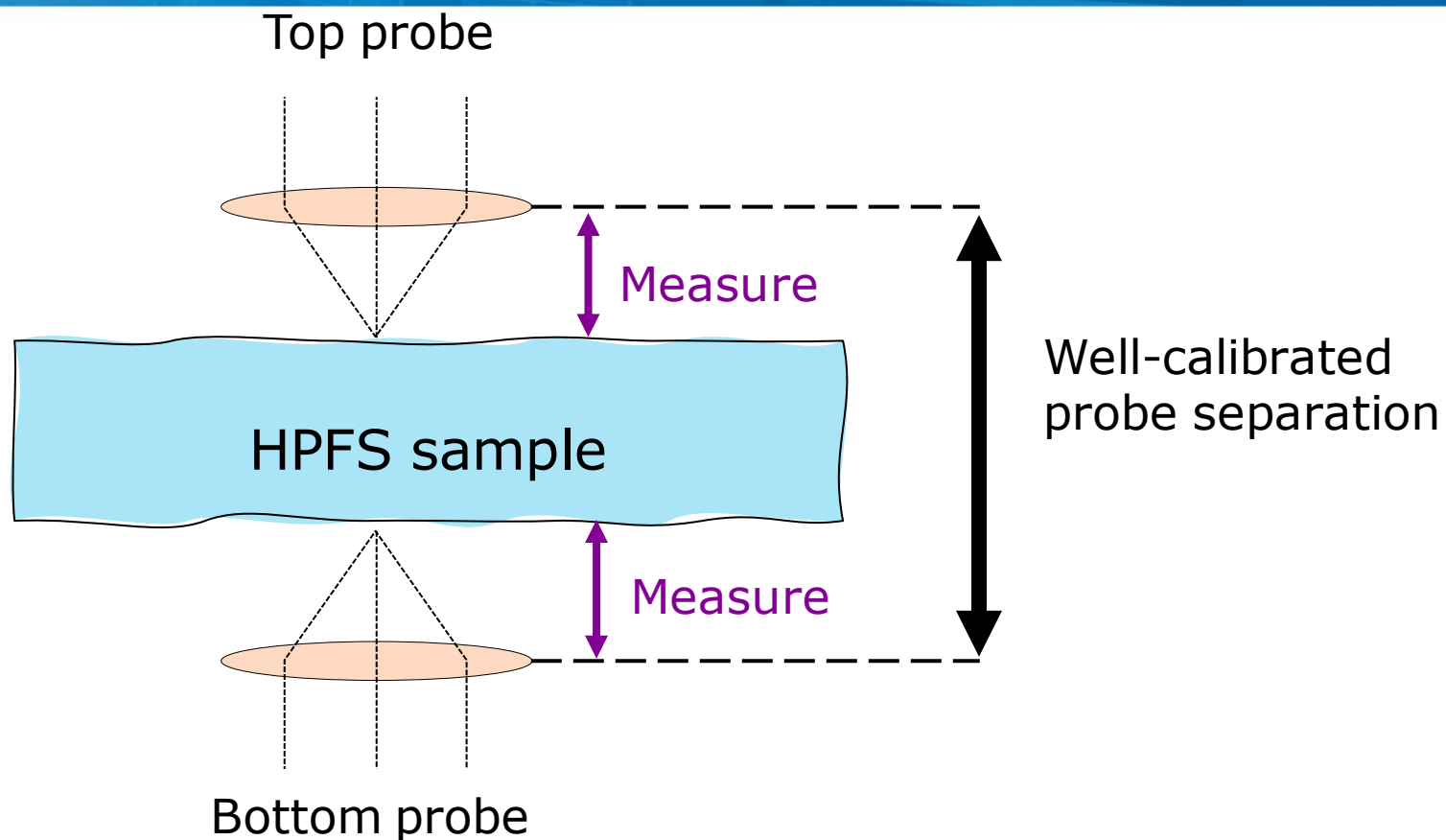
K	$0.71100 \pm 0.001 \text{ mm}$
S	$6.89650 \pm 0.001 \text{ mm}$
L	$4.69874 \pm 0.001 \text{ mm}$
R	$7.60784 \pm 0.0002 \text{ mm}$

Measurement uncertainties ($\leq 1 \text{ micron}$) $\ll$ our mean values

The sample dimensions are more difficult

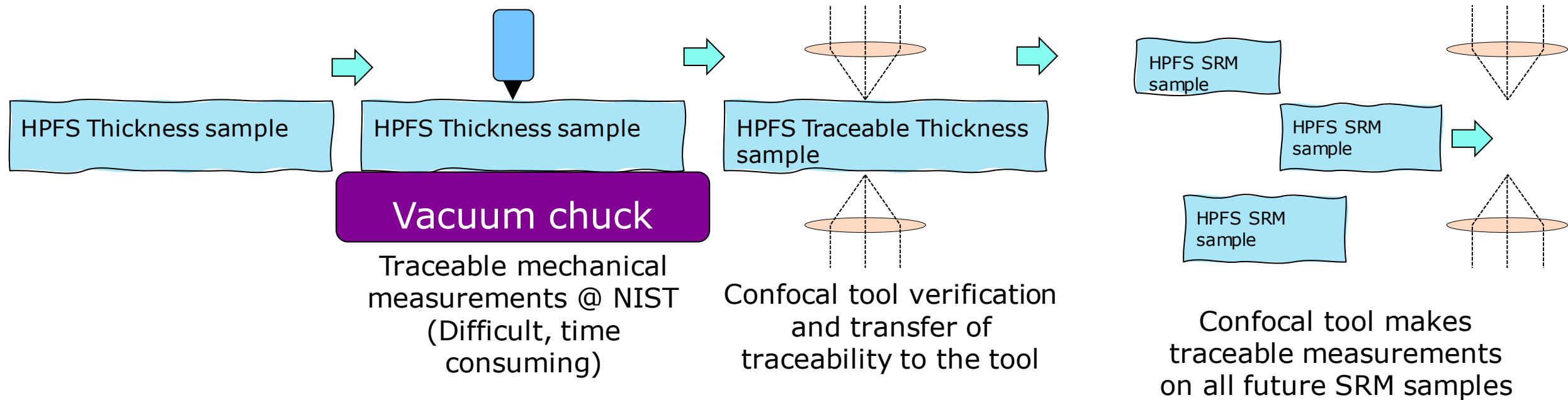
5

Measure
dimensions



Confocal white light sensors let us find both sample surfaces without assuming refractive index

We use the mechanical measurements to validate



Our final uncertainties are on the order of 100 nm
(0.067%)

The project overall and the progress we have made

Objective: Develop a standard for relative permittivity and loss tangent

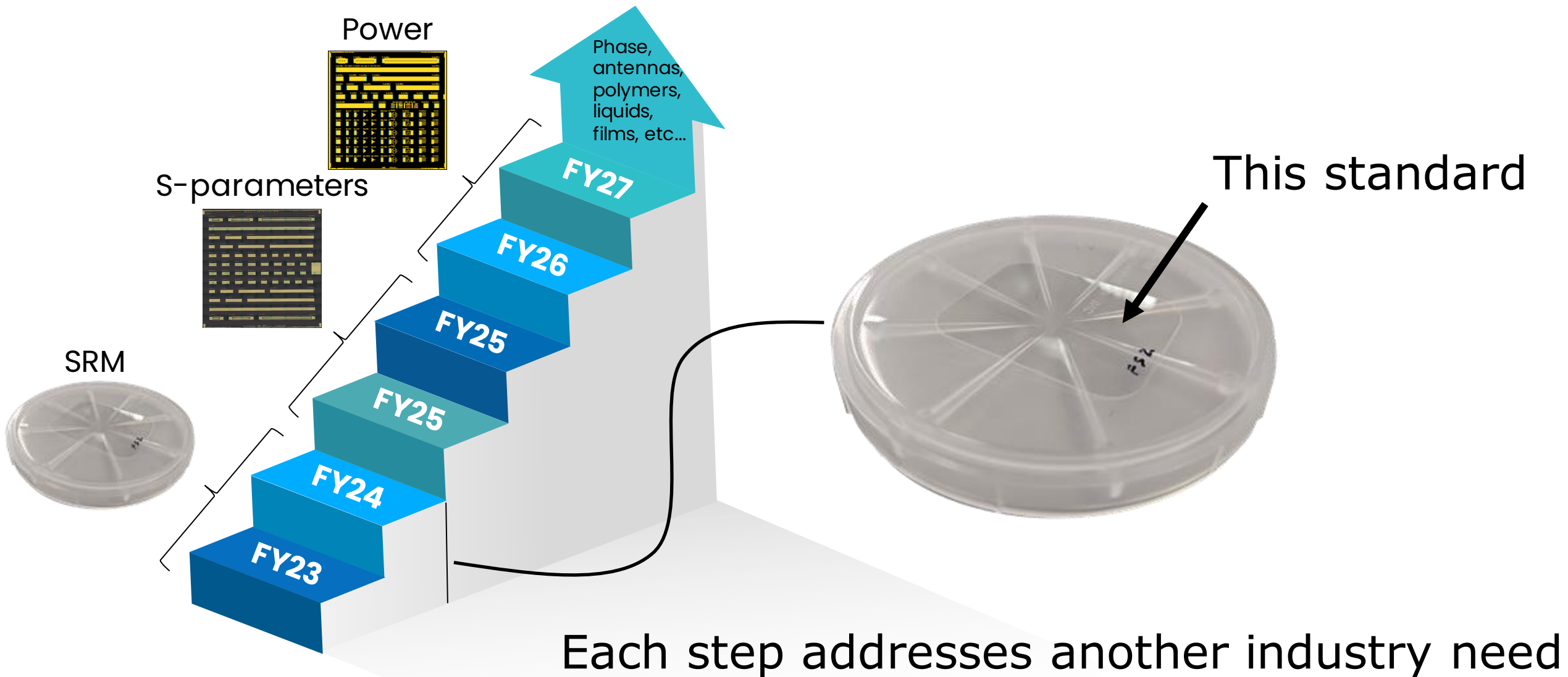
State-of-art: Resonant cavities for low-loss dielectric measurement

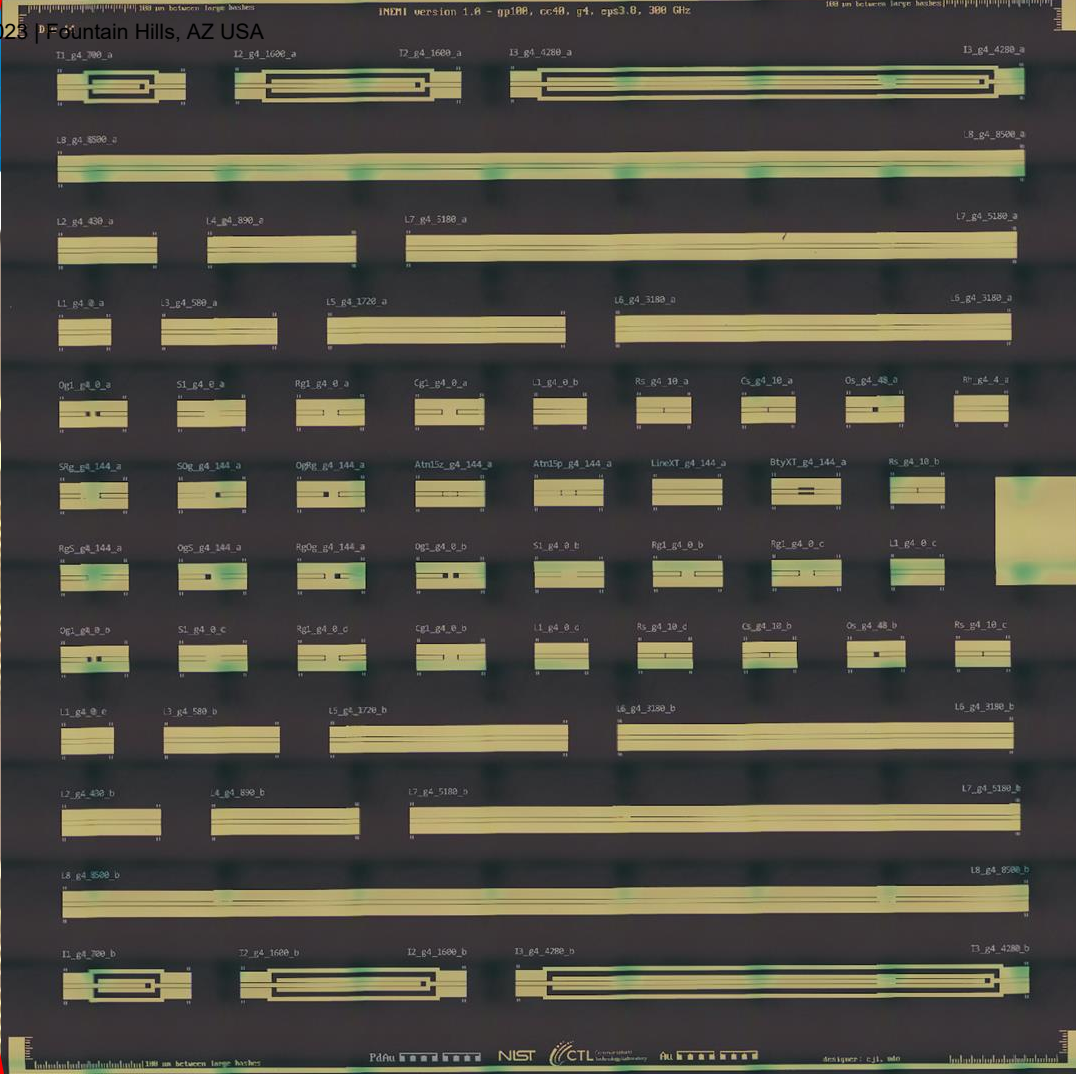
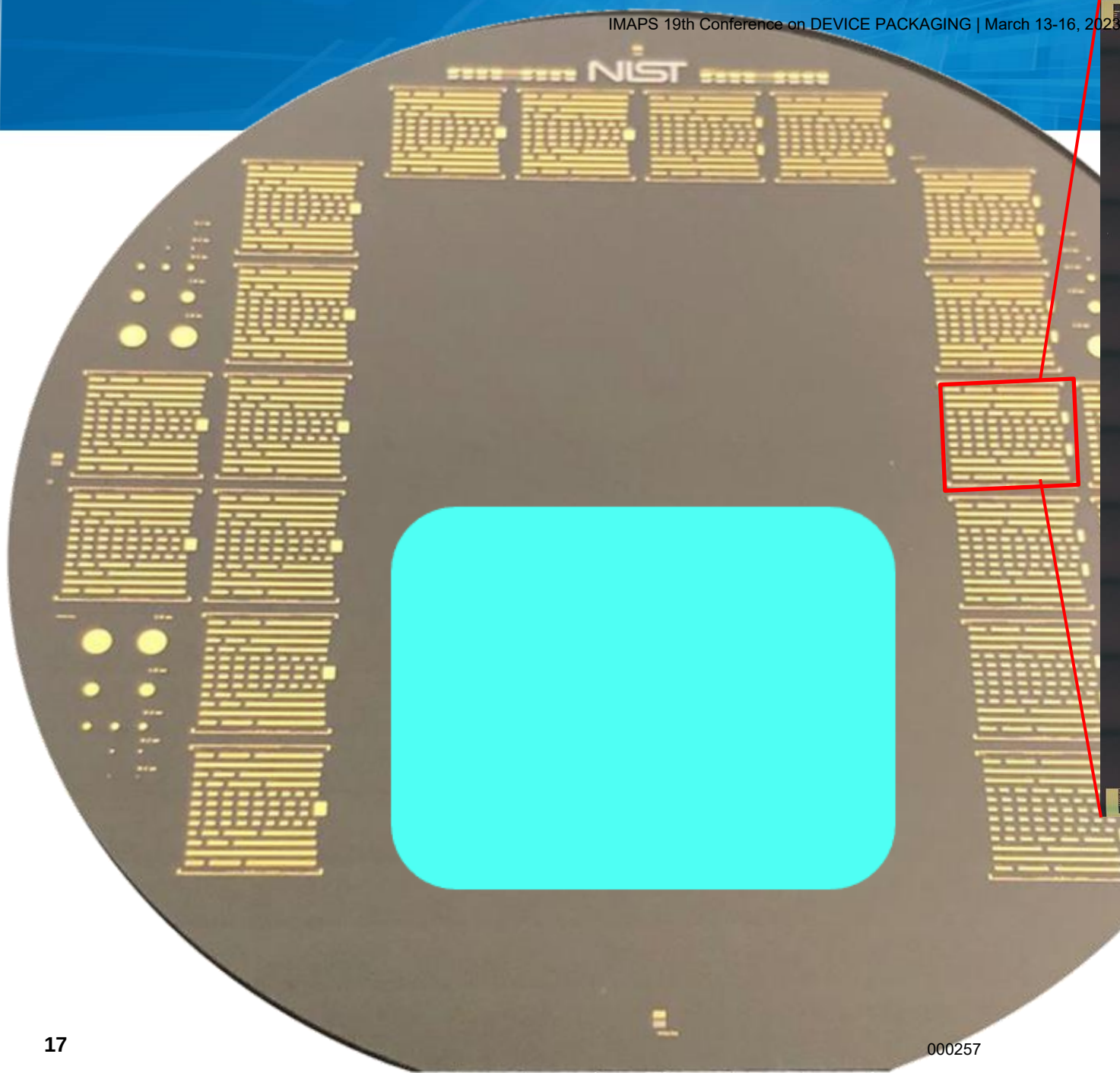
Key idea: High purity fused silica with ultra low TTV
Mode-matching theory including complete cavity geometry

Impact: Establishing a known 'right' answer for permittivity
Material acceptance testing and evaluating metrology

This standard is just the beginning

A staircase of future standards

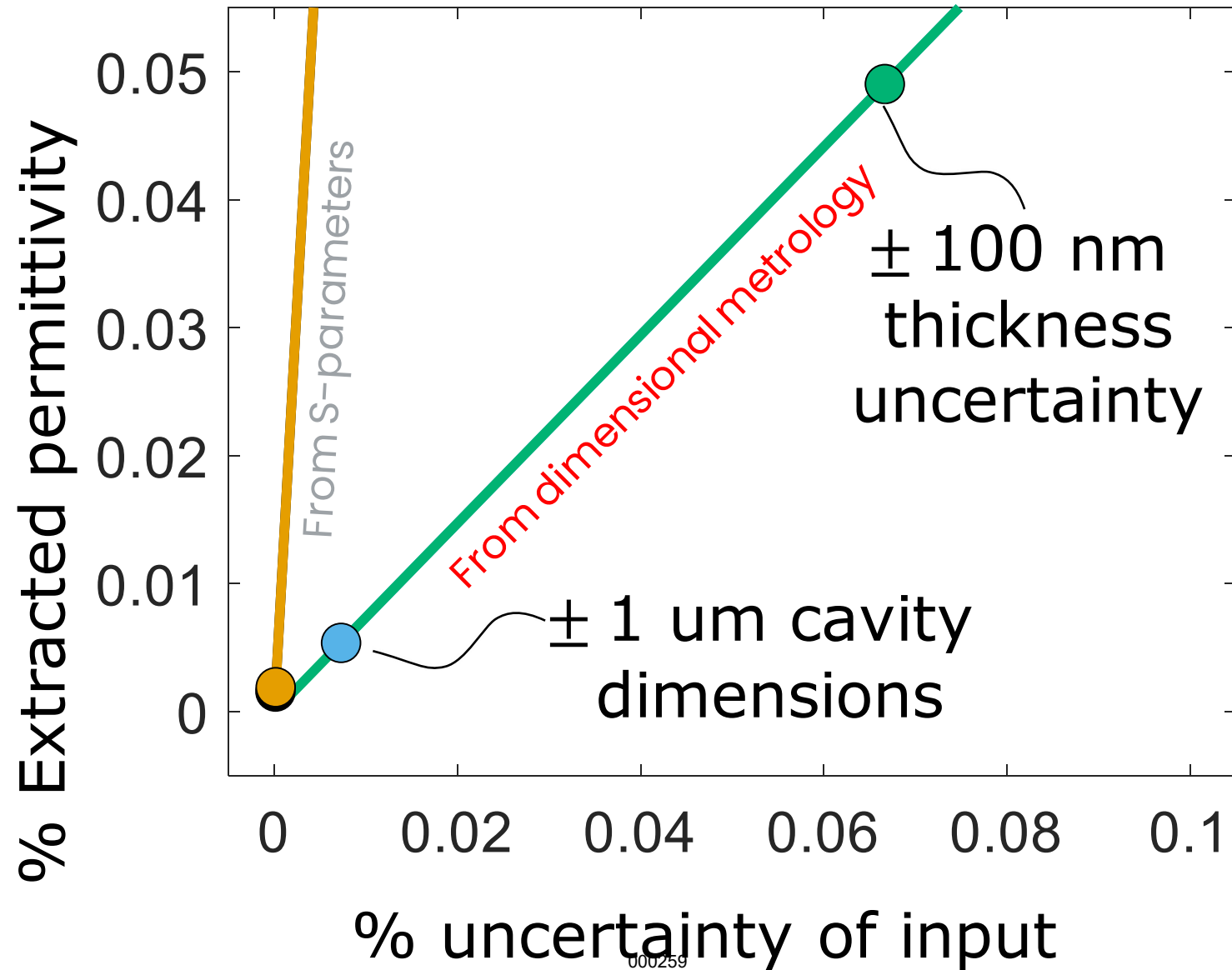




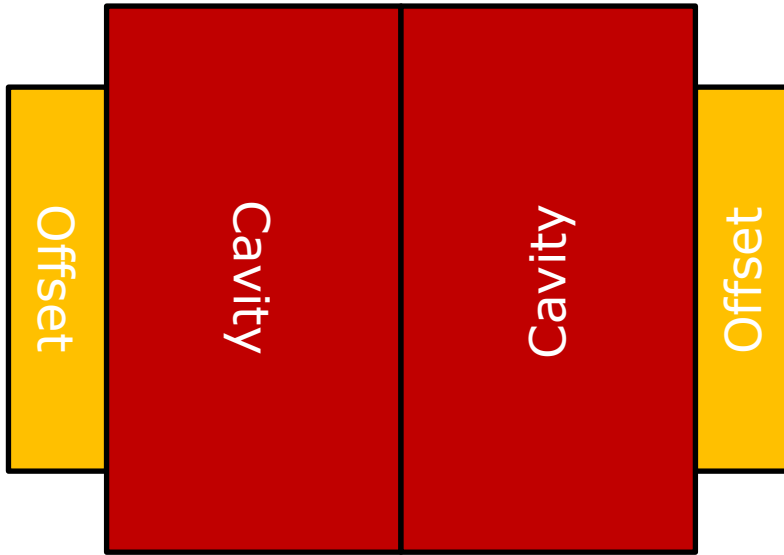
Thank you!



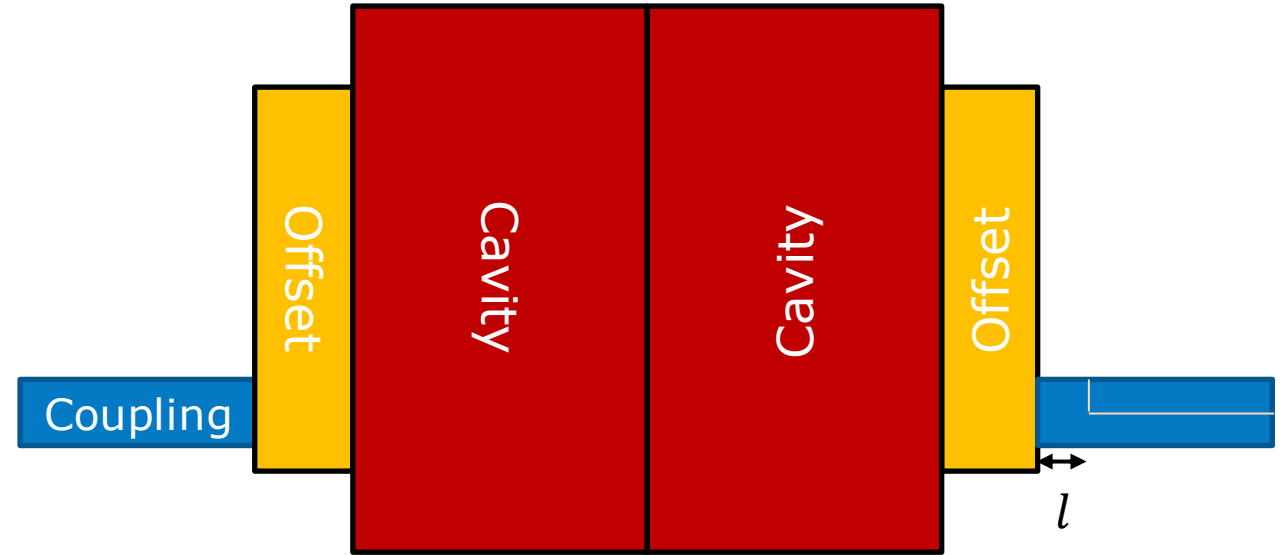
Our uncertainty is dominated by sample thickness



Mode-matching model:



Reality (i.e., with coupling):



Going to use HFSS to vary l

Anticipating two competing effects:

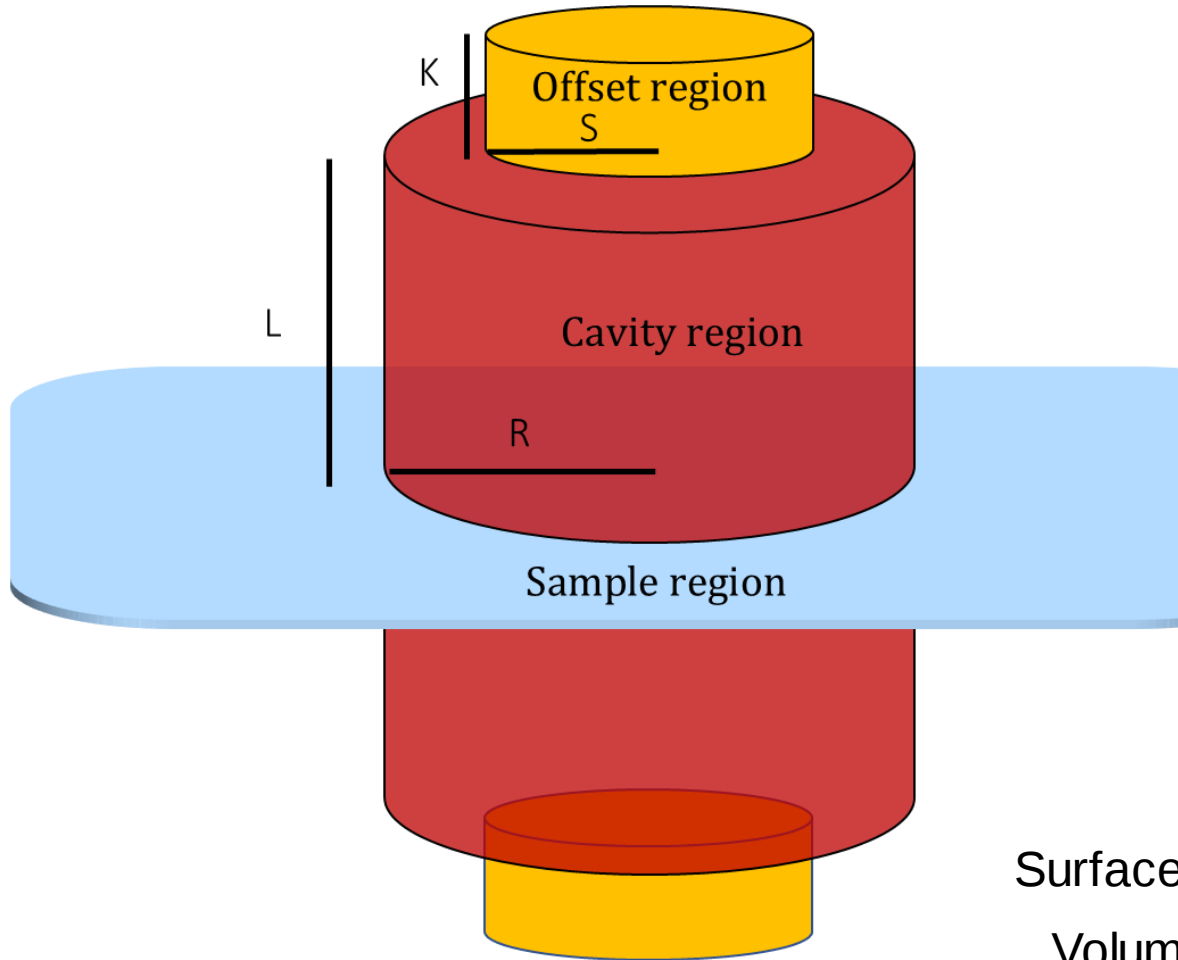
1. Increasing l will increase coupling (freq $\uparrow$)

Solution: fit to a network model with added inductors for coupling

2. Increasing l will increase the volume of the whole system (freq $\downarrow$)

Solution: More complicated theory (Mode-matching assumes symmetry about axis ☹)

Some of the gory details



Fields in upper offset:

$$E_{\phi UO} = \Sigma A_n U_n J_1(h_{nUO} \rho) \sin \left[p_{nUO} \left(z - K_U - L_U - \frac{d}{2} \right) \right]$$

$$H_{zUO} = -\frac{1}{j\omega\mu_0} * \Sigma h_{nUO} A_n U_n \sin \left[p_{nUO} \left(z - K_U - L_U - \frac{d}{2} \right) \right] * J_0(h_{nUO} \rho)$$

$$H_{\rho UO} = \frac{1}{j\omega\mu_0} * \left\{ \Sigma p_{nUO} A_n U_n J_1(h_{nUO} \rho) \cos \left[p_{nUO} \left(z - K_U - L_U - \frac{d}{2} \right) \right] \right\}$$

Fields in upper cavity:

$$E_{\phi U} = \Sigma B_n V_n J_1(h_{nU} \rho) \sin \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right] + C_n W_n J_1(h_{nU} \rho) \cos \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right]$$

$$H_{zU} = -\frac{1}{j\omega\mu_0} * \Sigma h_{nU} J_0(h_{nU} \rho) * \left\{ B_n V_n \sin \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right] + C_n W_n \cos \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right] \right\}$$

$$H_{\rho U} = \frac{1}{j\omega\mu_0} \Sigma p_{nU} J_1(h_{nU} \rho) \left\{ B_n V_n \cos \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right] - C_n W_n \sin \left[p_{nU} \left(z - \frac{L_U}{2} - \frac{d}{2} \right) \right] \right\}$$

Fields in sample:

$$E_{\phi S} = \Sigma D_n X_n J_1(h_{nS} \rho) \sin[p_{nS}(z)] + F_n Y_n J_1(h_{nS} \rho) \cos[p_{nS}(z)]$$

$$H_{zS} = -\frac{1}{j\omega\mu_0} * \Sigma h_{nS} J_0(h_{nS} \rho) * \{ D_n X_n \sin[p_{nS}(z)] + F_n Y_n \cos[p_{nS}(z)] \}$$

$$H_{\rho S} = \frac{1}{j\omega\mu_0} \Sigma p_{nS} J_1(h_{nS} \rho) \{ D_n X_n \cos[p_{nS}(z)] - F_n Y_n * \sin[p_{nS}(z)] \}$$

Surface currents → Power dissipated through each surface ($P_{surface}$)

Volume integrals → Average energy stored in each region (W_{region})