

6G Hardware System Design and Packaging Needs

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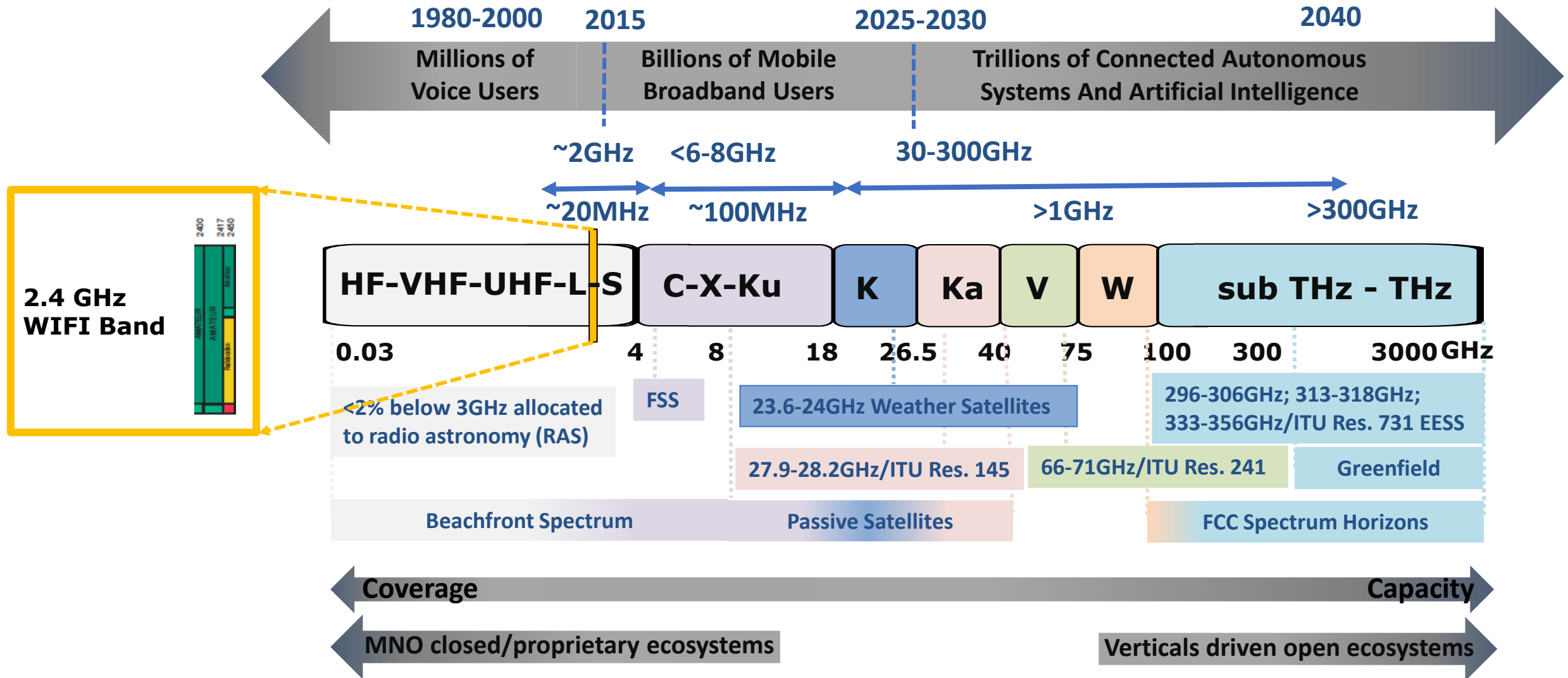
- 20 years of experience in power, RF/mmWave and sensor packaging
- Expertise in passive components, 3D package integration, wireless biosensors
- 360 publications, which include 8 patents.
- More than 25 best-paper awards.
- Co-advised ~40 MS and PhD students
- Former Chair of Nanopackaging Technical Committee, Former EPS Representative of IEEE Nanotechnology Council, IEEE Distinguished Lecturer in Nanotechnology for 2020-2021, Associate Editor for IEEE Nanotechnology Magazine and Transactions of Components, Packaging and Manufacturing Technologies (T-CPMT), General Chair for 3D PEIM 2023
- PhD from Rutgers University in 1999 in Ceramic Engineering,
- ME from the Indian Institute of Science, Bangalore
- BS from the Indian Institute of Technology, Kanpur (1993)



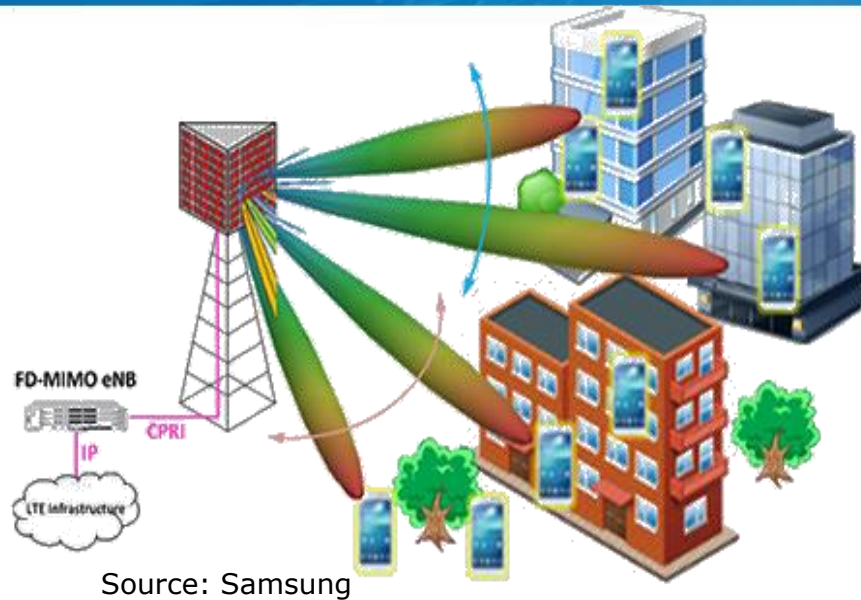
Outline

- Beamforming Architectures
- Reconfigurable intelligent surfaces
- Package Integration Trends
 - Antenna-in-package
 - Embedded filters, power dividers
 - Tunable FSS

Spectrum Sharing Evolution



Research Areas in 5G, 6G, and Beyond



New Market Demands

Amazingly Fast

Great Service in a crowd

Super Real-time & reliable communications

Ubiquitous "things" Communicating

Areas of Research:

- 1) ***MIMO beamforming architectures***
- 2) ***Advanced techniques to address spectrum coexistence and improve spectral efficiency and interference mitigation***
- 3) Ultra-Wideband (UWB) systems
- 4) RF front ends: frequency agile, very small size, weight area, and power efficient (SWAP)
- 5) SMART Antennas
- 6) Millimeter-wave systems
- 7) RF-digital Transceivers
- 8) Integrating Machine Learning and Artificial Intelligence in RF design
- 9) Communication in contested environment

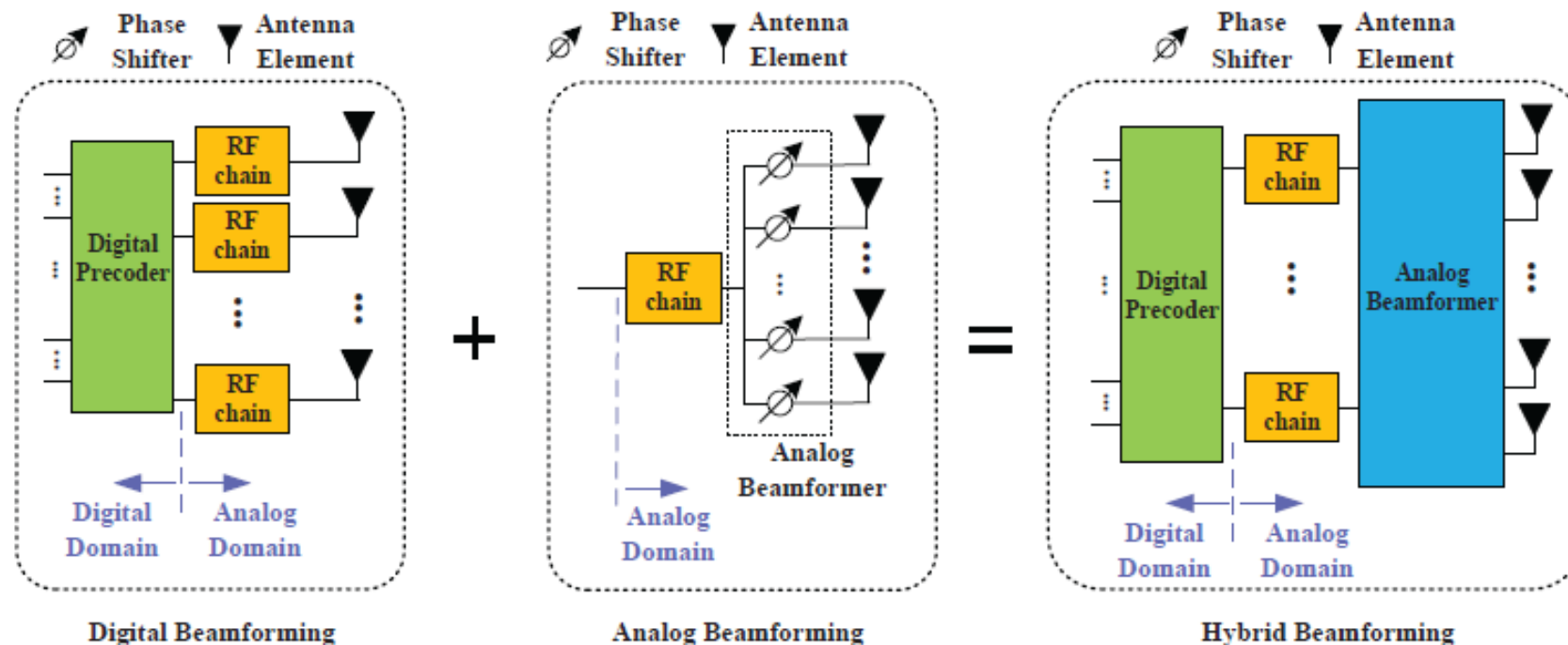
R1: Beamforming Transceiver Architectures

Analog beamforming:

- Antenna phase is adjusted through the phase shifters in the analog domain
- Limits flexibility of control and impairs the beamforming performance and capacity improvement

Digital beamforming:

- Realizes any linear transformation of multiple signal streams from the digital baseband to the antenna elements
- Provides a greater degree of freedom
- Unaffordable to be applied in massive-MIMO systems due to the high-power consumption and high system cost



Hybrid Beamforming

Hybrid beamforming methods jointly optimize the analog and digital beamformers to maximize the achievable rate based on cost-performance trade-off.

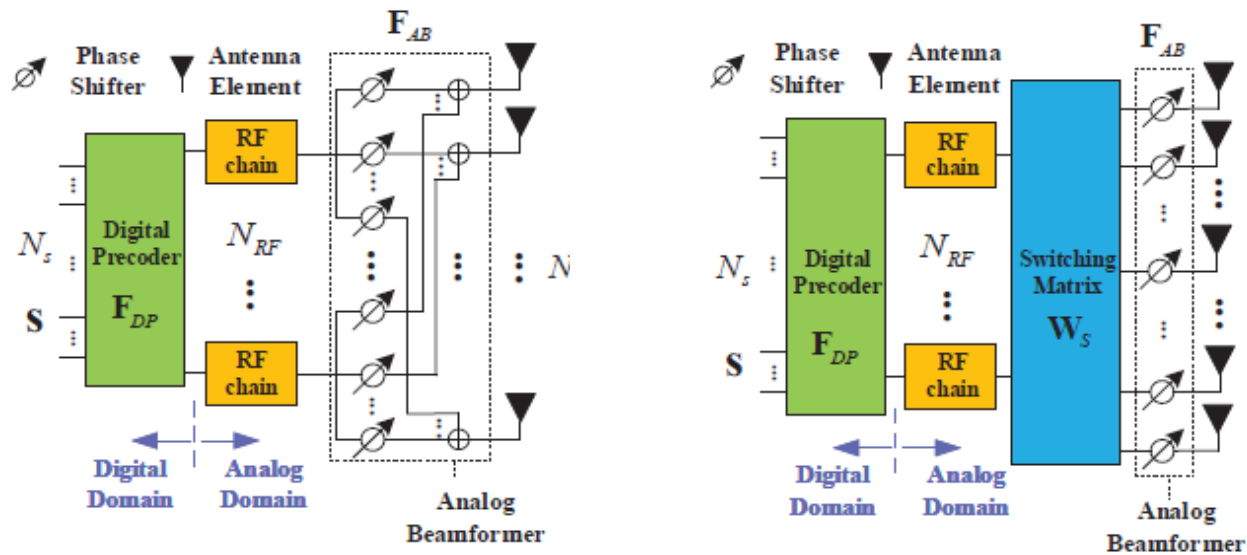


Fig: Fully-connected vs Dynamically connected HB^[1]

Advantages

- Enables mmWave Massive MIMO communications with $1000 \times$ capacity enhancement
- Reduces Capital Hardware Cost by reducing the required number of RF chains at TX and RX sides
- Provides Energy Efficiency by potentially reduces the downlink and uplink transmit power through coherent combining and an increased antenna aperture
- Reduces Operational Cost when employing large array of antennas by allowing the use of low-cost RF amplifiers in the milliwatt range,

Challenges

- Constant magnitude constraint enforced by analog phase shifters
- Finite quantization of analog phase-shifters results in programming problems
- Limited CSI availability leads to difficulty in UL and DL channel estimation
- Limited to narrowband operation

Wideband Beamforming

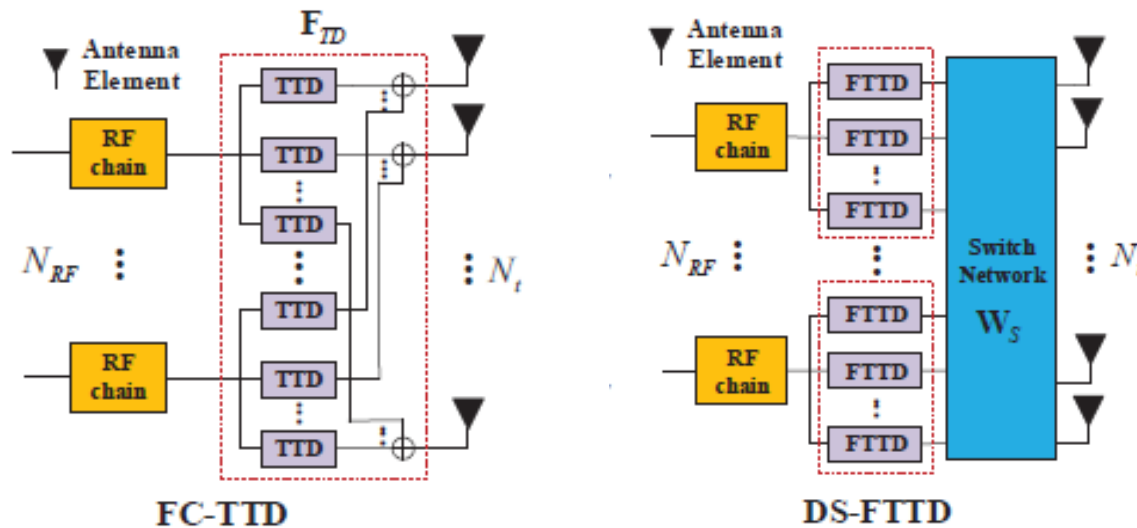


Fig: Fully-connected vs Dynamic sub-array TTD architectures^[1]

Spatial wideband effect

- Signal envelope received by different antenna elements might not belong to the same symbol
- Phased array cannot effectively combine the signals
- Dividing the baseband into several sub-bands and concurrently processing each sub-band that has a lower symbol rate by the digital beamformer.

- TTD architecture addresses both spatial wideband and frequency-wideband effects
- Compensates for the effects of space and frequency by imposing a true time delay on the signal at each antenna element
- Suffers from high hardware complexity and cost in analog domain as there are many RF chains and the dynamic range requirement is extremely high
- Easily be realized in the digital domain

Frequency wideband effect

- Signal components of different frequencies arrive at the array with different phase differences
- Same phase compensation cannot simultaneously maximize the beam gains at all frequencies
- Beam pattern changes with the frequency of the signal (beam squint effect)

Reconfigurable Intelligent Surfaces – Assisted Joint Beamforming

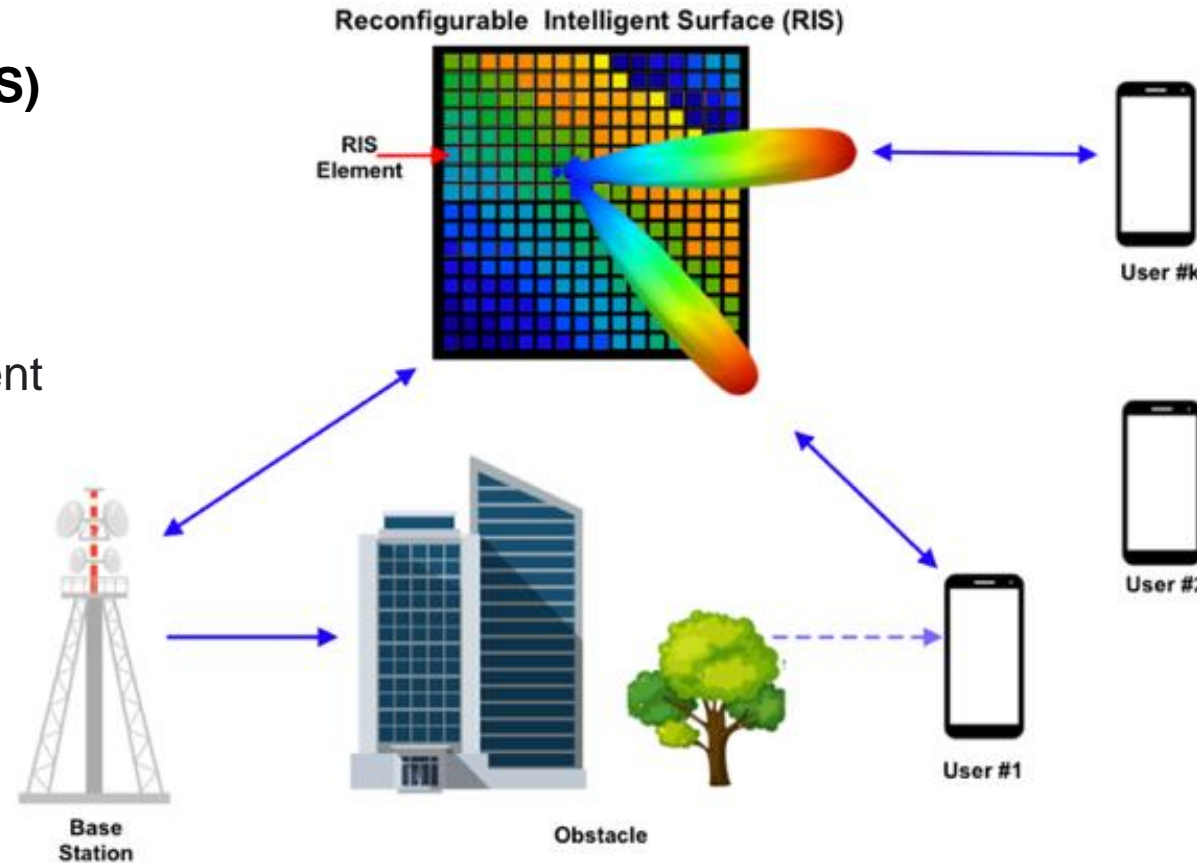
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Small wavelengths at 5G/6G mm-Wave frequencies are subject to path losses and multipath scattering leading to beam blockage

Reconfigurable Intelligent Surfaces (RIS)

supersede relay performance using large apertures with simple circuitry.

- ✓ Spectrally more efficient
- ✓ RIS reduce hardware complexity.

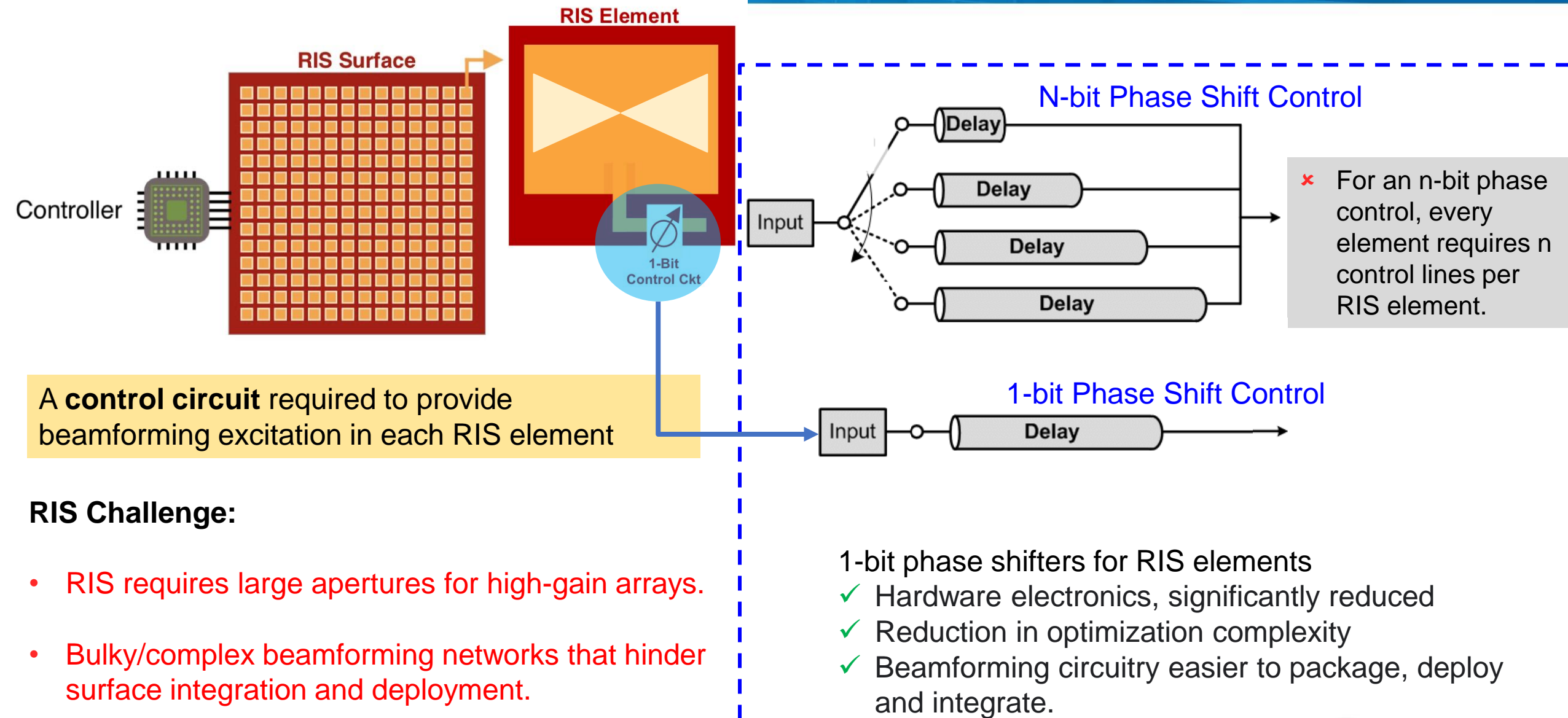


Alternative Technology: Relays

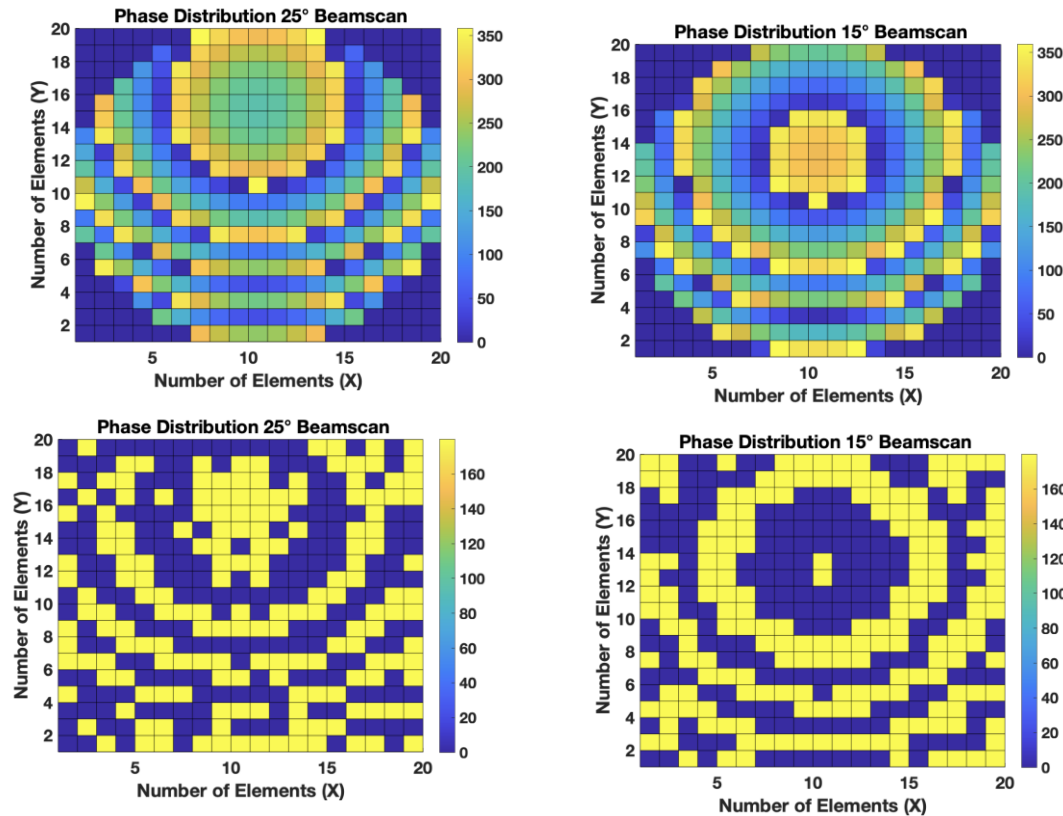
- ✗ A dedicated power source per relay
- ✗ Reception and re-transmission circuitry
- ✗ Signal processing complexities.

Goal: Beamforming and adaptive nulling using RIS via a very simple circuitry (in terms of SWAP-C)

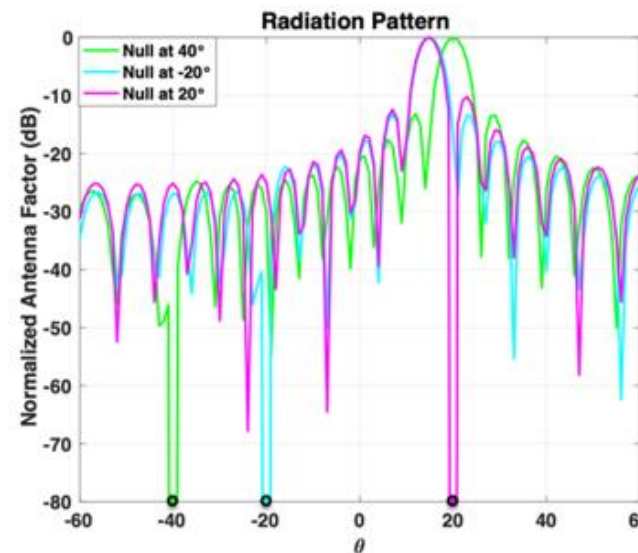
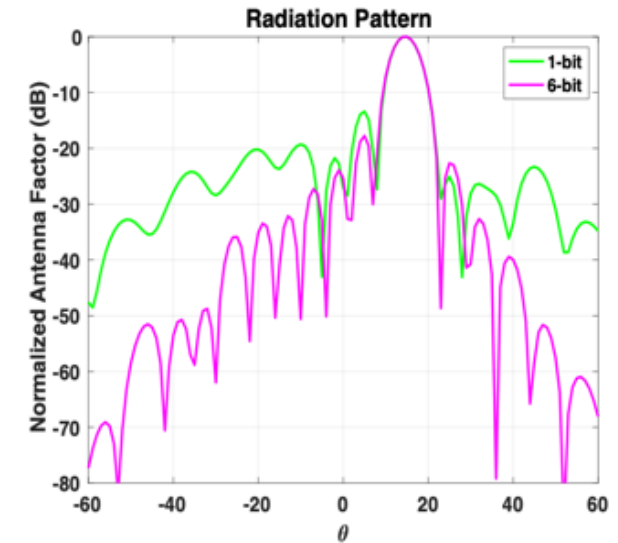
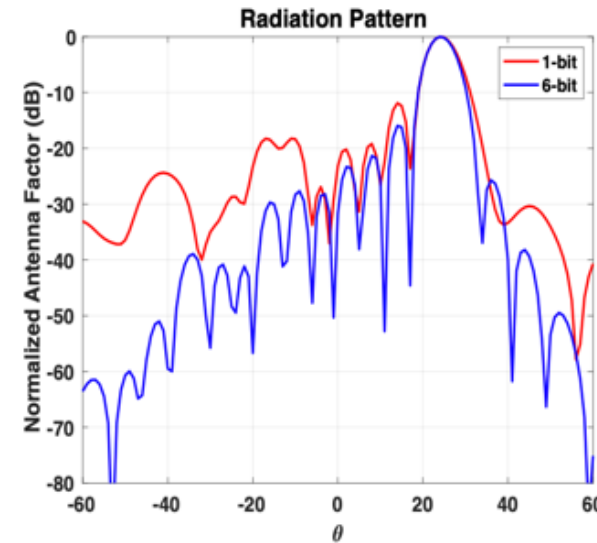
RIS Beamforming with 1-bit Phase Shifters



Comparison Between 1-bit vs. 6-bit Phase Distributions



Direction	Directivity 6-bit	Directivity 1-bit
25°	20dB	16dB
15°	23dB	19dB



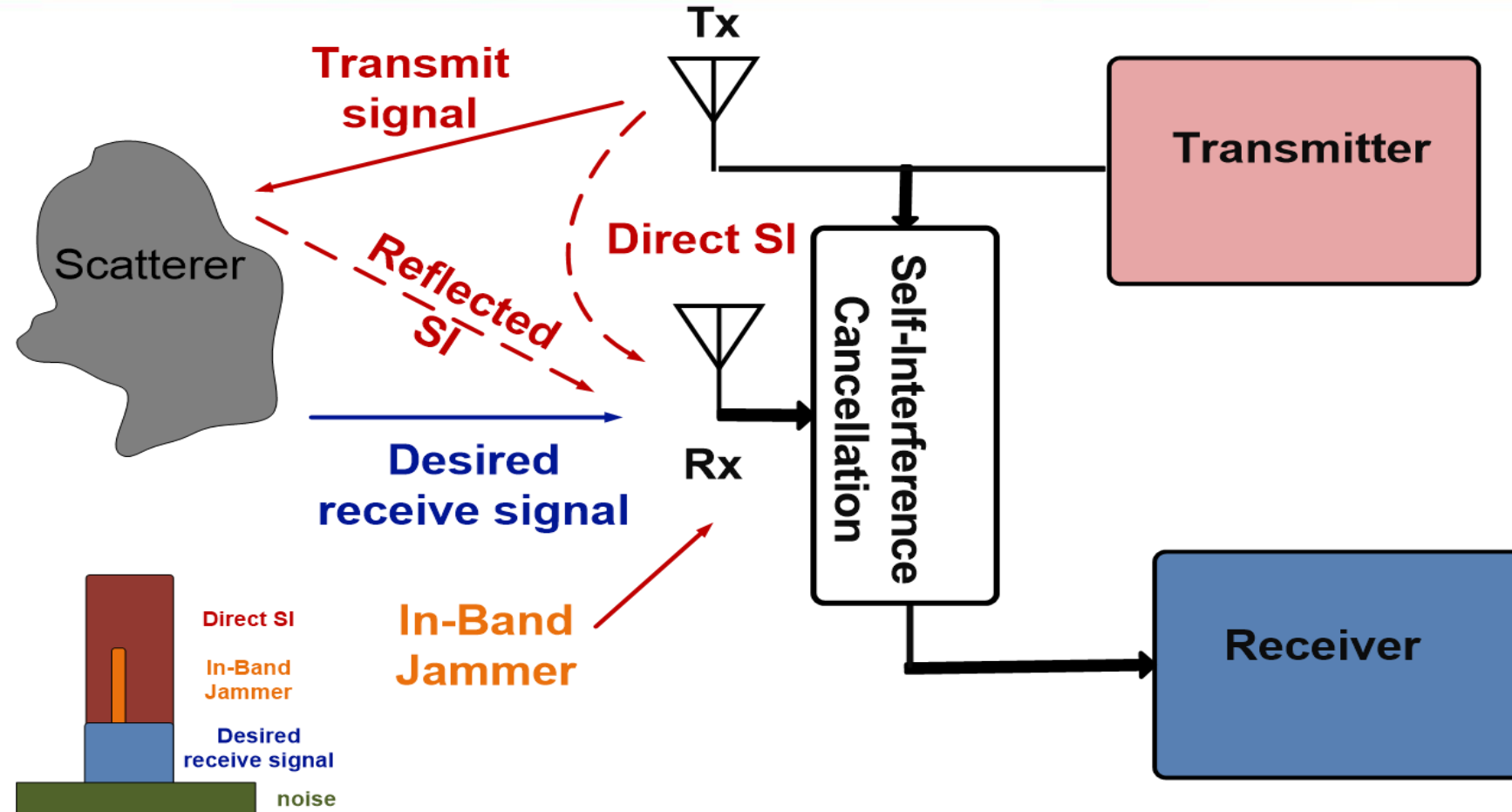
- **2400 digital control lines** required using a 6-bit network.
 - **Only 400 digital control lines** are needed for a single bit configuration.
- **6-fold reduction in DC power.**

Interference mitigation techniques for next-generation radios

RF systems are prone to:

- 1) In-band External Jammers
- 2) High Power self-interference in simultaneous transmit and receive systems.

Direct self interference and in-band jammers cause receiver desensitization



More efficient use of the available spectrum requires:

- 1- Self-Interference cancellation through Simultaneous Transmit and Recieve (STAR) to double spectral efficiency
- 2- Interference/Jamming mitigation (~40 dB) through channel coding and modulation

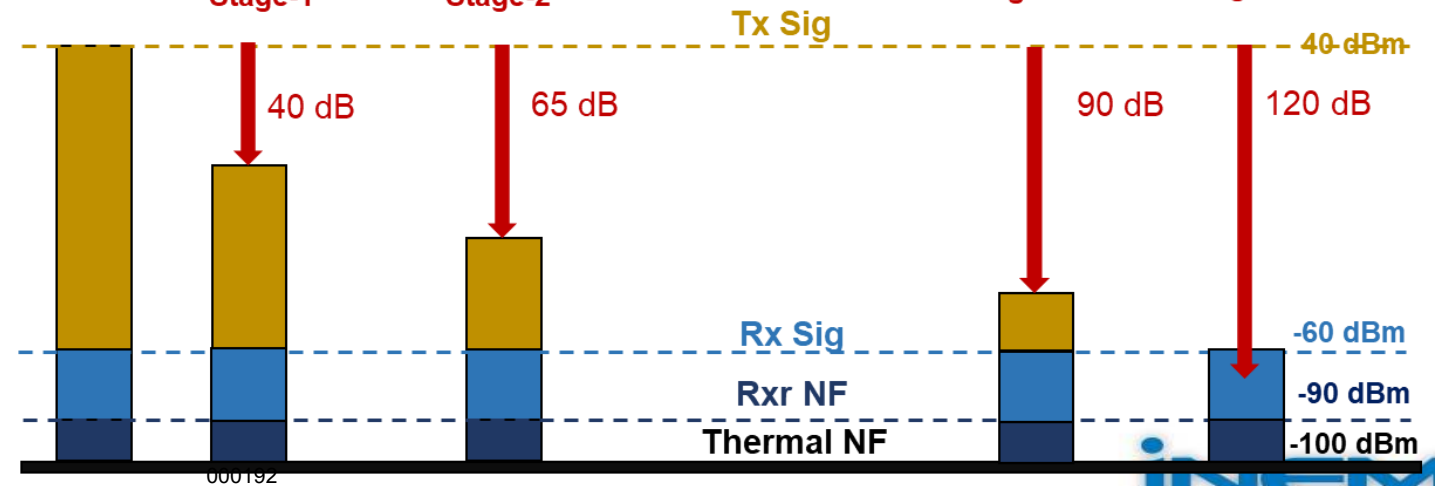
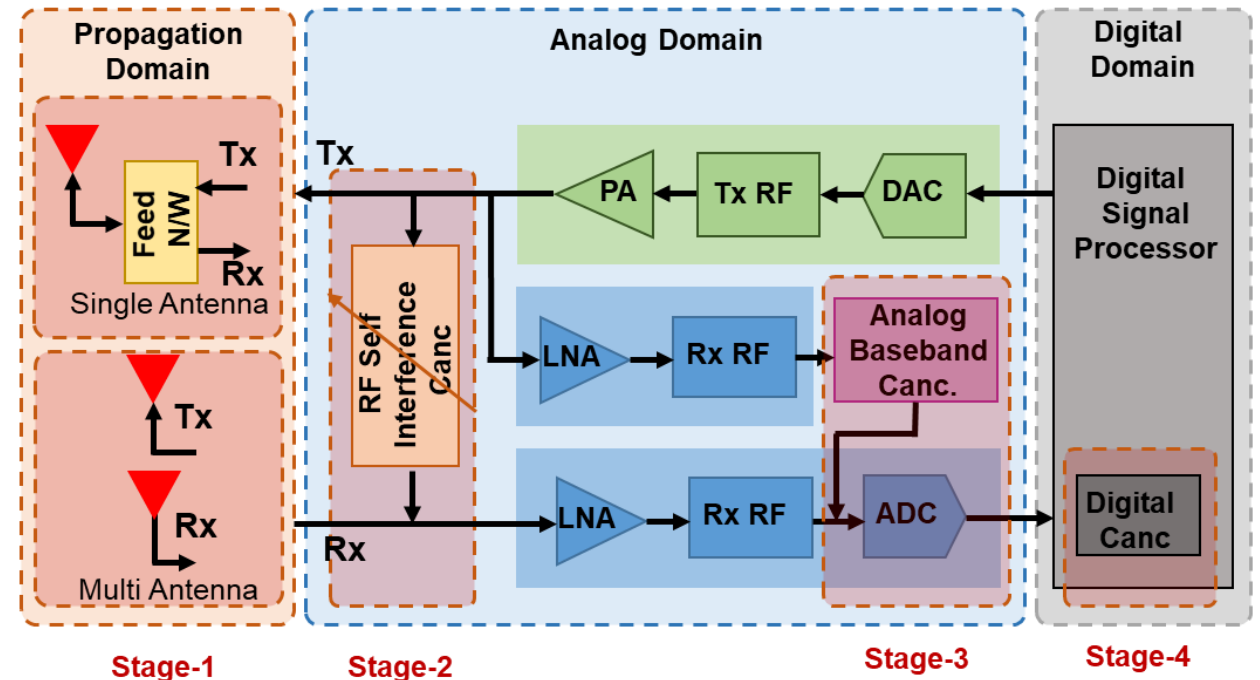
R2: Advanced Techniques To Address Spectrum Coexistence And Improve Spectral Efficiency

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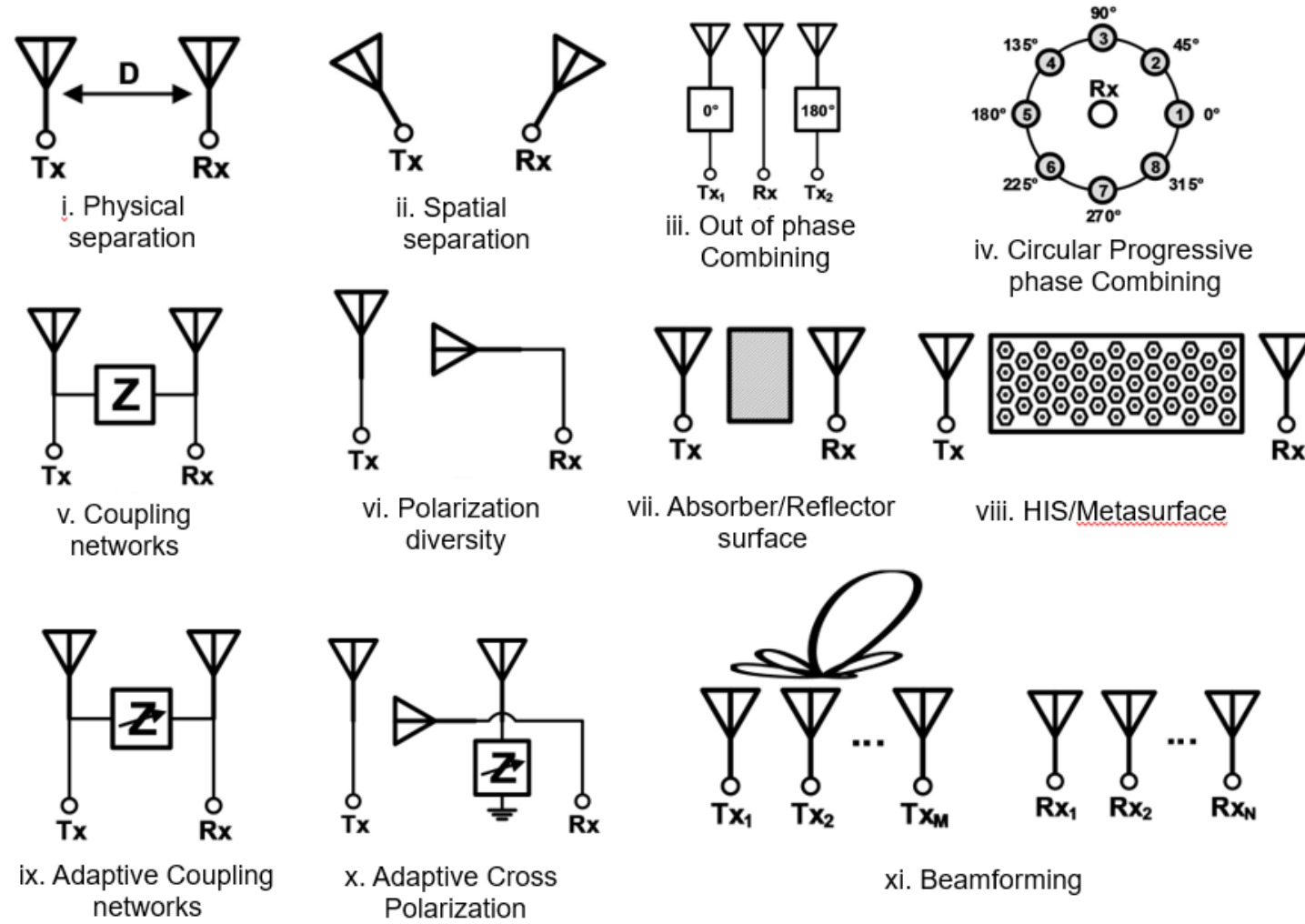
Different STAR architectures considered to account for Tx coupling on to Rx chain:

- All components should be suppressed as much as possible
- > 50 dB suppression of main signal required in this case
- > 30 dB suppression of non-linear components, including harmonics and Tx noise
- Tx signal, Tx nonlinearities (harmonics + noise) are to be suppressed equally

With proper Self-Interference cancellation, STAR achieves **twice the capacity** as compared to TDD/FDD.

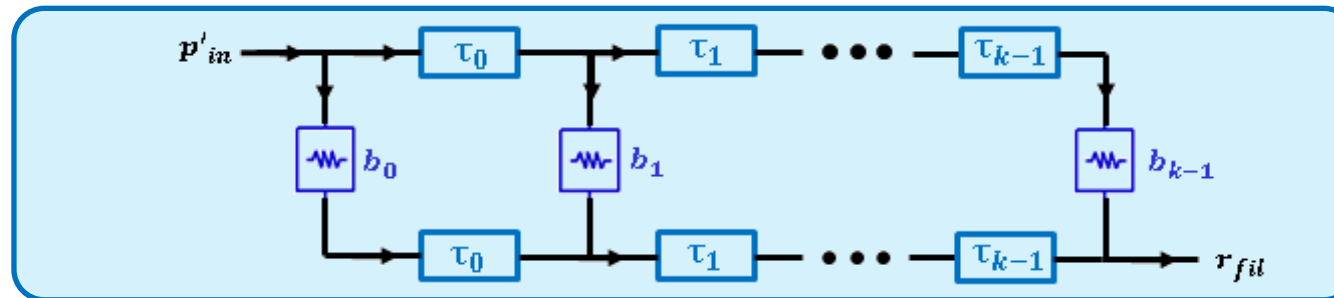
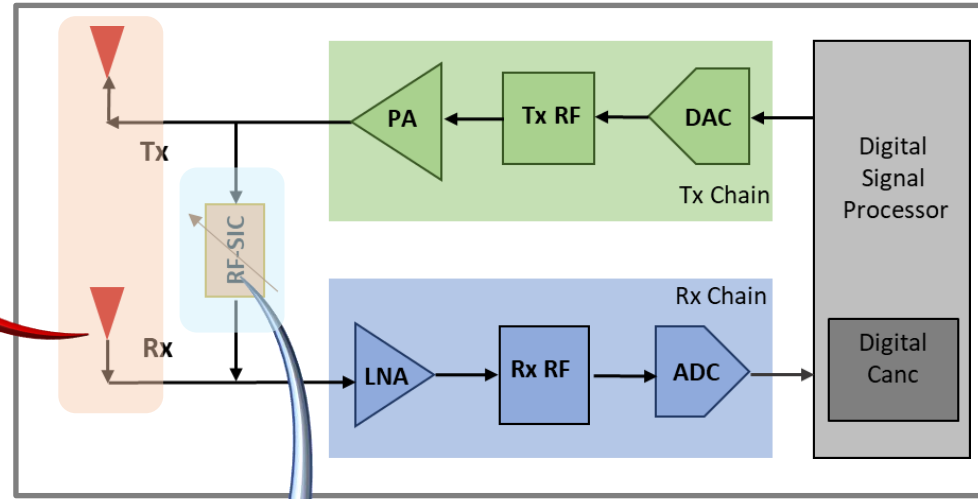
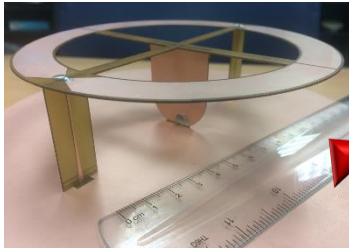


Stage-1: Different Cancellation Techniques in a Multi-antenna System



Stage-2: Design of Multitap RF-SIC Filter to Match Antenna Response

RF-SIC Filter Design



- Estimate proper filter order
- Optimize variable and realize as transmission lines the optimized W and L values
- Attenuators are also optimized accordingly

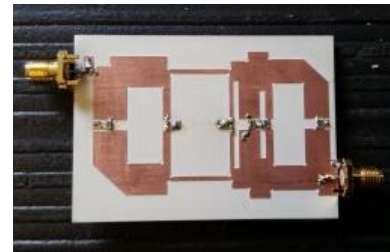
Measured RF Filter Response of Mutlitap FIR Filter Prototypes

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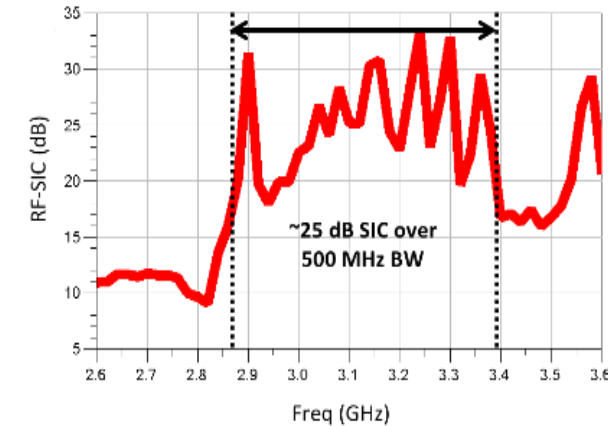
Accomplished

- 1) **Fabricated and tested prototype 1**
 - Instantaneous operational bandwidth of 500 MHz
 - 6 filter taps with variable microstrip L and W used
 - Measured RF cancellation of ~25dB over 500 MHz
- 2) **Fabrication of 1GHz RF filter with:**
 - Employed filter banks to realize wideband operation
 - Reduced foot print
 - 12 taps to operate over 1 GHz

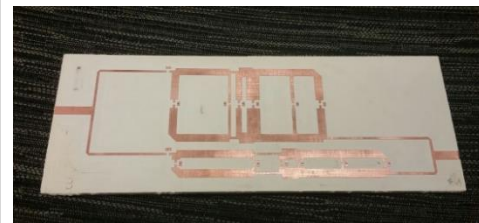
1st Prototype – 0.5 GHz



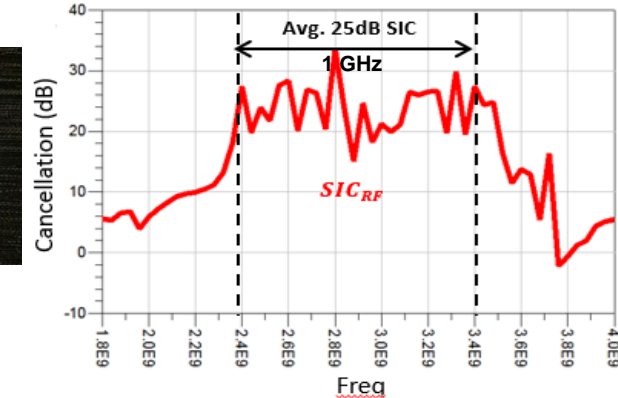
Measured RF Cancellation



2nd Prototype – 1 GHz



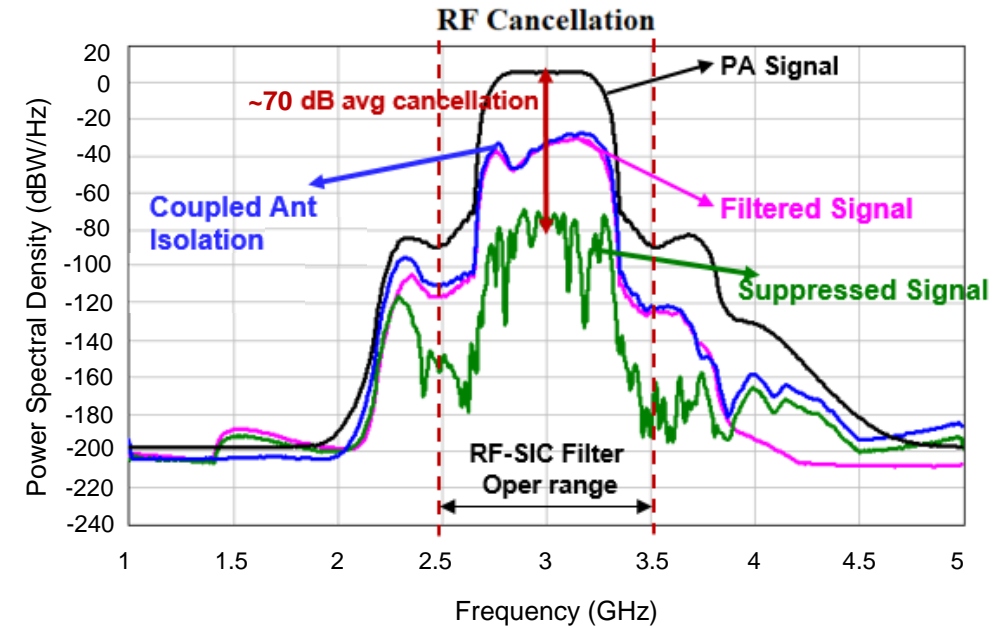
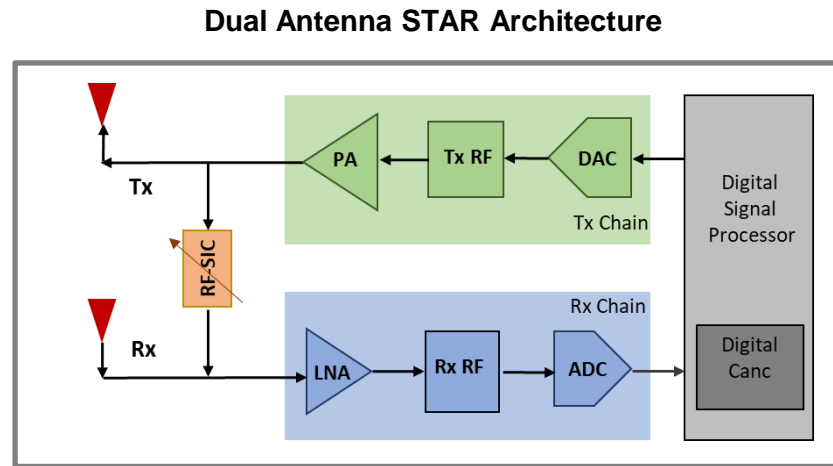
Measured RF Cancellation



For the first time, we demonstrate RF cancellation of ~25 dB over 0.5 and 1 GHz

Combined 2-stage cancellation of STAR transceiver Over 1 GHz bandwidth

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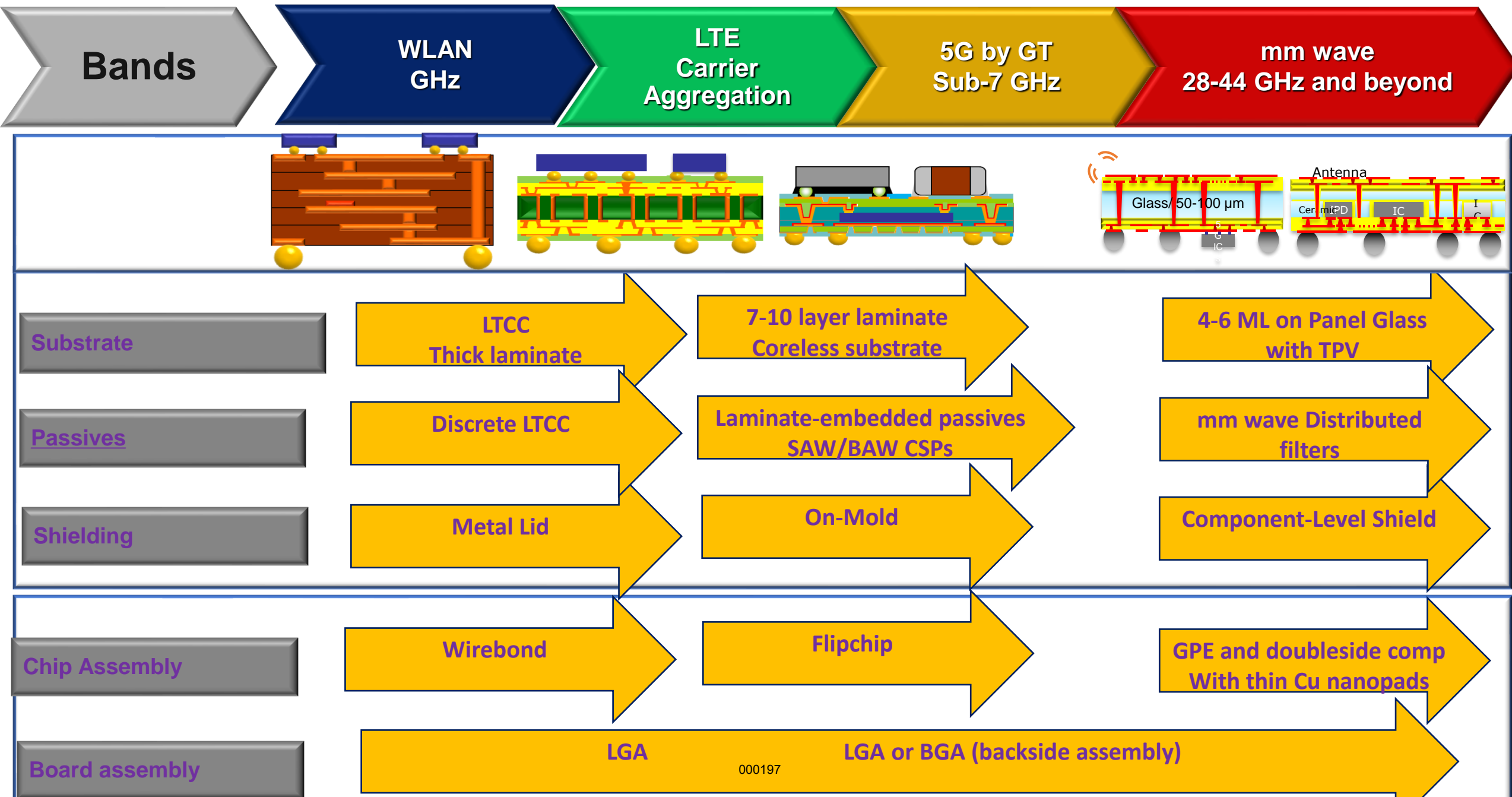
1) Design of 1GHz RF cancellation filter with:

- Filter banks using 12 taps
- Conformal design
- Achieved cancellation of ~25dB over 1GHz

2) Modified STAR architecture to account for Tx noise influence of the cancellation:

- Tx noise cancelled by sourcing a part of it directly to RF filter
- RF filter designed to include mutual coupling effect from nearby elements

RF Module Evolution



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Substrates and Design Rules

- High-density, impedance-matched (2-5%) and low-loss transmission lines:
 - High-density RF and digital in the same package
 - Smooth surface for low losses:
- Create thinfilm components:
 - Decoupling for high-speed mm wave lines
 - Tunable and reconfigurable components
- Seamless layer-to-layer and 3D interconnects
 - Impedance-matched TPVs
 - Minimal signal discontinuities and reflections with ultra-fine vias and pads
 - Better termination of E-fields with multiple ground vias or arrays – Lower noise coupling with less mutual and self-inductance
 - Minimal ground bounce and resonance effects with small clearances (less intrusion) in power planes
- Precision circuitry for impedance matching
- Package- and board-level reliability
- Availability in 30-100 microns
- Large-area panel processing

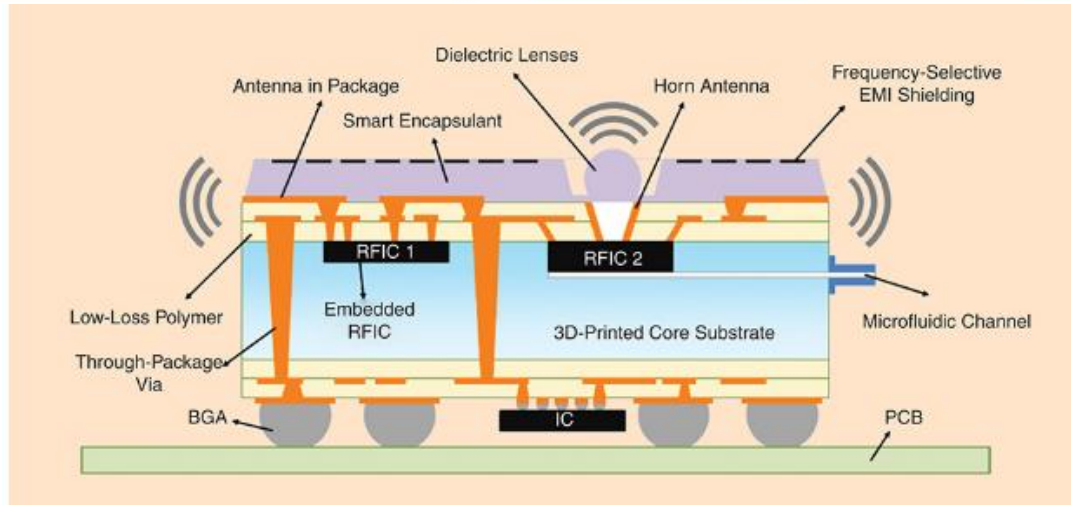
	LTCC	Laminates	Glass
Substrate thickness	>500 mm	>300 mm	<150 mm
Feature size with 5% precision	100 mm	40-50 mm	10-20 mm
Through-via diameter and pitch	100mm/ 300mm	100 mm / 300 mm	25 mm/ 50 mm
Through-thickness variation	>25 mm	>10 mm	0.5 -1 mm
Manufacturing Panel size (metric for cost)	150-200 mm000198	510 mm	510 mm

Materials: LTCC to Laminates, FOWLP and Glass

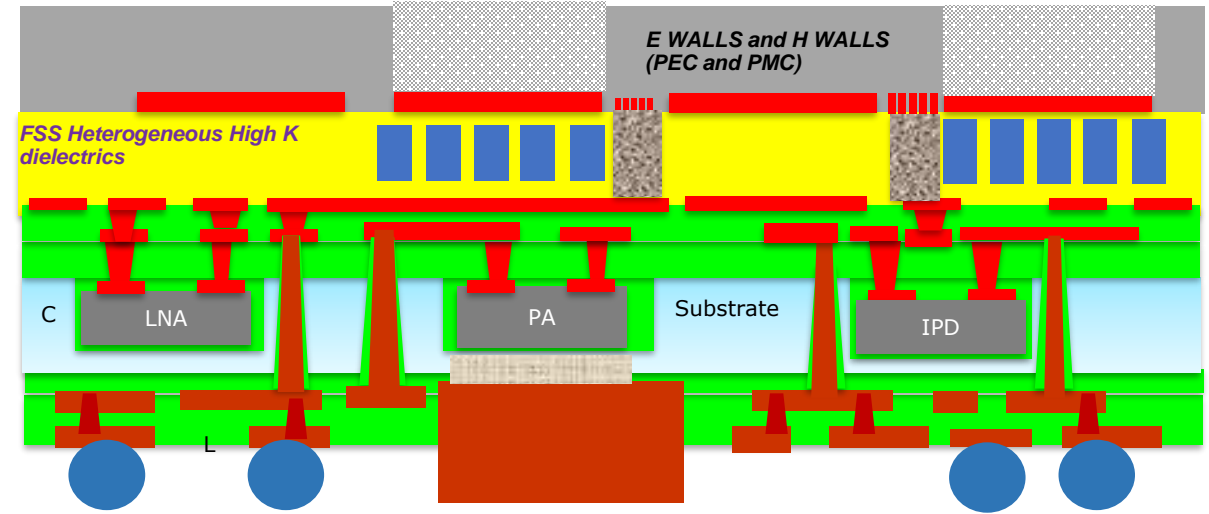
- Glass is a promising candidate for next-generation substrate material for 5G applications

	Flip-Chip			Chip-Embedding	Flip-chip & Embedding
Characteristic	PCB-based	LTCC	Organic laminates	FO-WLP	Glass
Material Properties					
Relative dielectric constant (ϵ_r)	4	5 – 10	2.9-3.2	3.68	2.7 – 7
Loss tangent $\times 10^4$ ($\tan\delta$ @ GHz)	20 @ 10	12 @ 10	40 @ 60	80 @ 58	3 – 50 @ 10
Surface roughness (nm)	300-5800	177	400-600	> 1000 on EMC	<1
Coefficient of thermal expansion - CTE (ppm/K)	17	5.5 – 7.2	17	30 (EMC)	3-8.5
Dimensional stability - Young's Modulus (GPa)	21 – 24	90-150	10-40	22	50-90
Water absorption	0.1%-0.25%	0	0.040 %		0
Process Challenges					
Multi-layer process alignment					
Small-feature patterning					
Thin substrate reliability	Warpage		Warpage		Cracking

5G/mmWave Package Integration



- High-density and low-loss transmission lines:
- Ultra-fine vias and TPVs for seamless 3D interconnects
- Precision circuitry for impedance matching
- Smooth surface for low losses

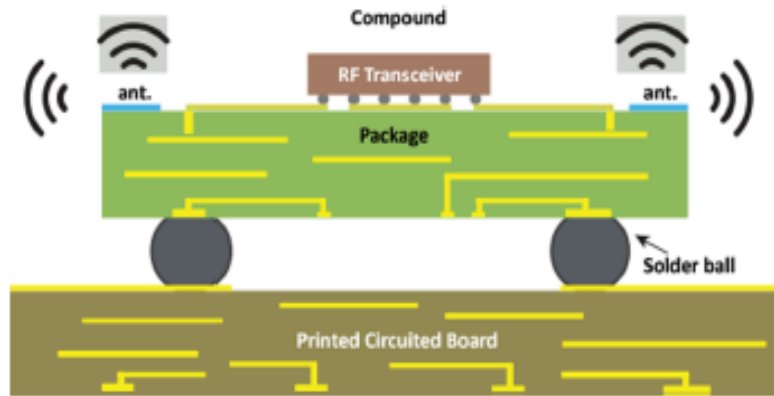


- RF and digital in the same package
- Advanced antenna array for wideband and gain
- Embedded FSS for improved performance
 - Heterogeneous high-K superstrates as lenses,
 - E walls, H walls, AMCs
- Package- and board-level reliability
- Large-area panel processing

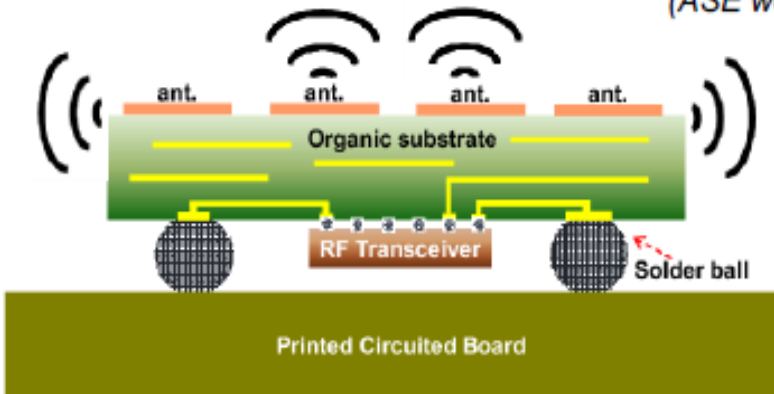
Antenna-in-Package (AiP)

Flip-chip AiP (FC-AiP)

5G mm-Wave package for Apple's iPhone 12 from ASE



(ASE website)



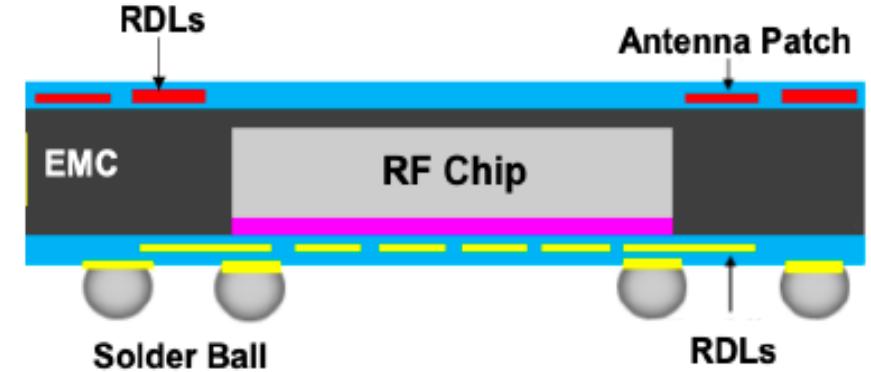
- (+) Low cost, Mature process
- (-) Form-factor, Package parasitics



Fanout AiP (FO-AiP)

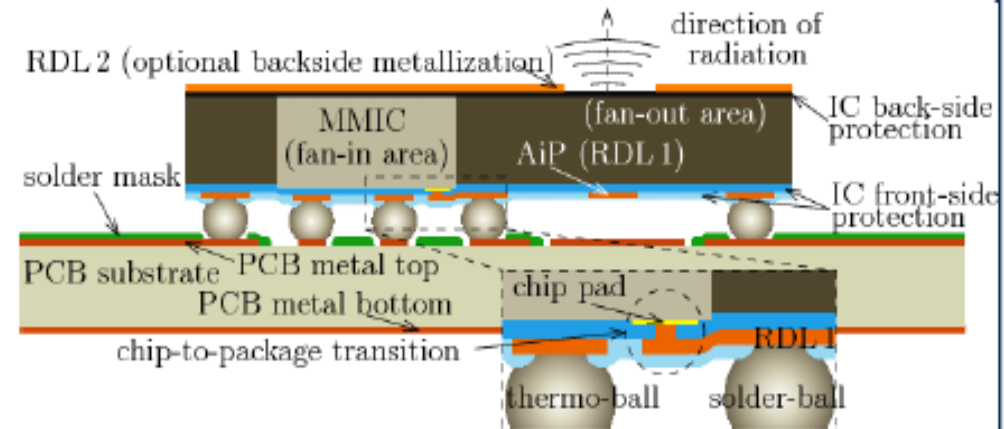
TSMC InFO-AiP
for 5G mm-wave

(TSCM, ECTC'18)



Infineon eWLB
for radar

(Infineon EWLB,
EUMC '18)

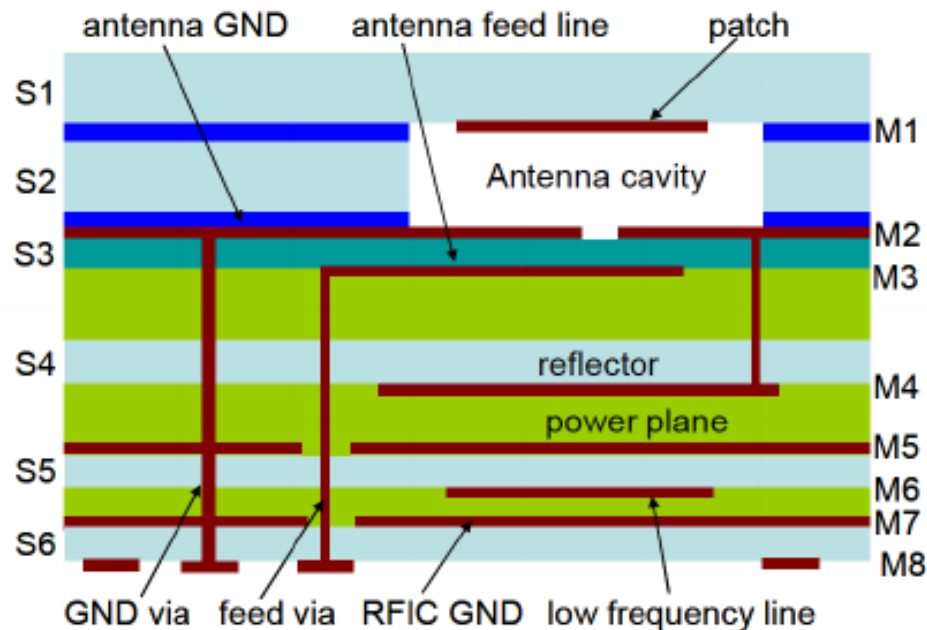


- (+) Lower cost
- (+) Form factor
- (+) Performance (no bump parasitics)

Antennas: Planar, Stacked and Broadband

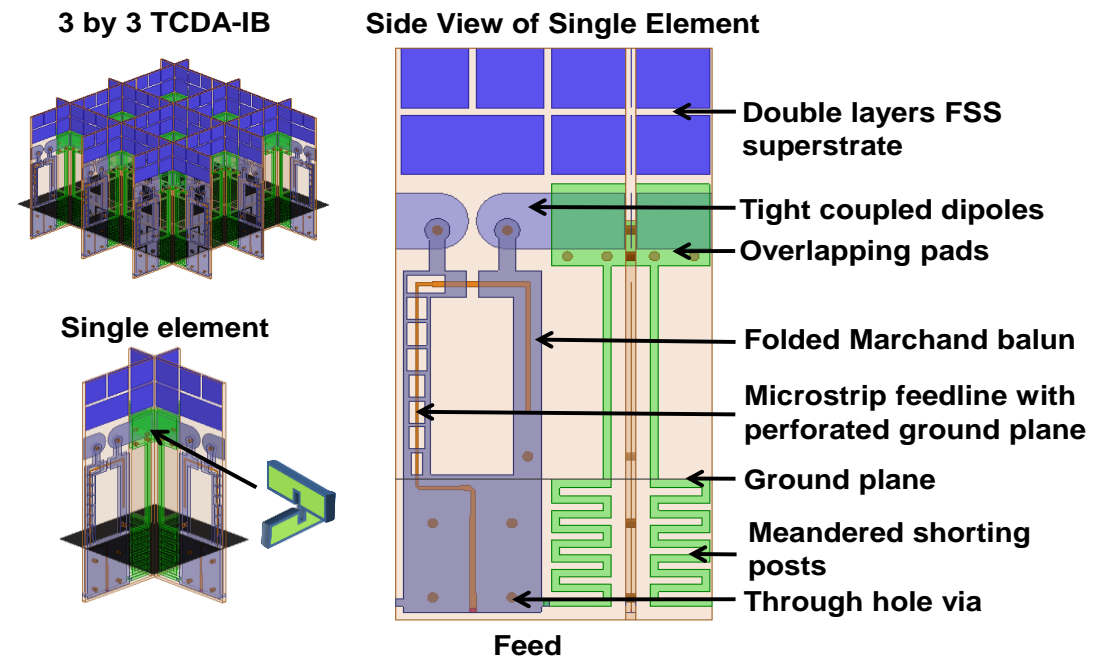
For resonator antennas, bandwidth enhancement with:

- Irregular shapes
- Stacked antennas with different materials
- Air cavity: mitigates surface waves and increases bandwidth
- Fractal antennas, where the golden ratio is maintained
- Defected ground structures where a rectangular defect is etched at the center of the ground plane
- Via-array for isolation



For aperture antennas:

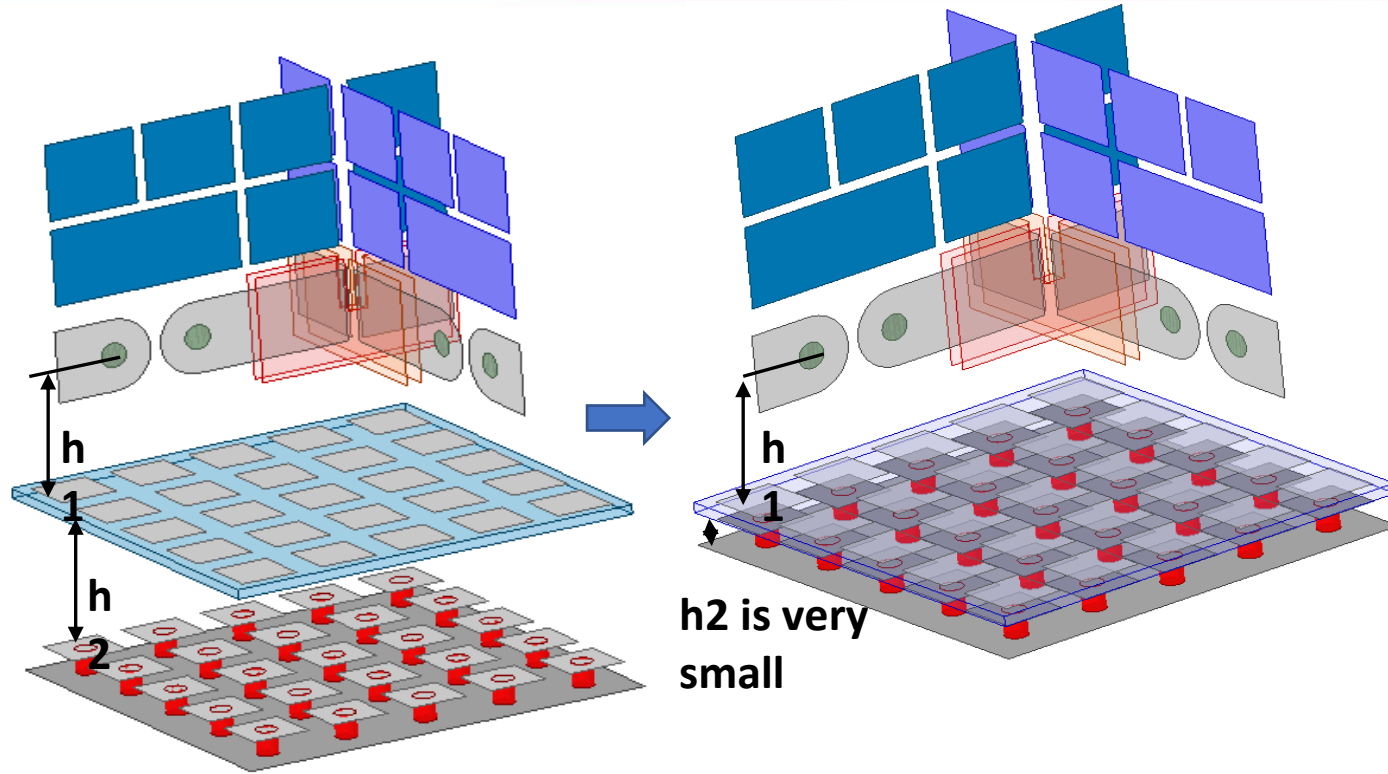
- Enhanced inter-element capacitive coupling to increase the bandwidth
- Integration of Marchand Balun to further expand bandwidth.
- RSS (resistive substrate card loading) for increasing the bandwidth,
- Introduction of FSS superstrates



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Ground Height Reduction with Printed Resistive FSS

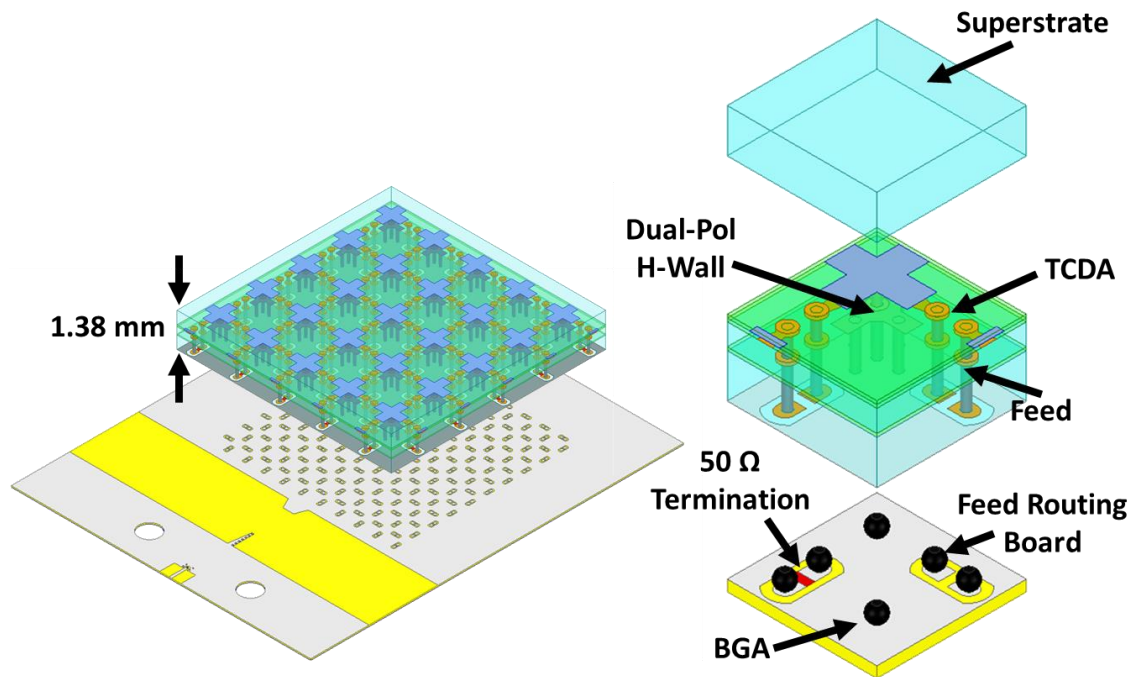
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- As HIS operating bandwidth have some limitation, TCDA ground height reduction is limited upto the semi-resistive FSS.
- TCDA ground height can be reduced significantly as the phase of the reflected wave can be controlled using HIS ground planes.

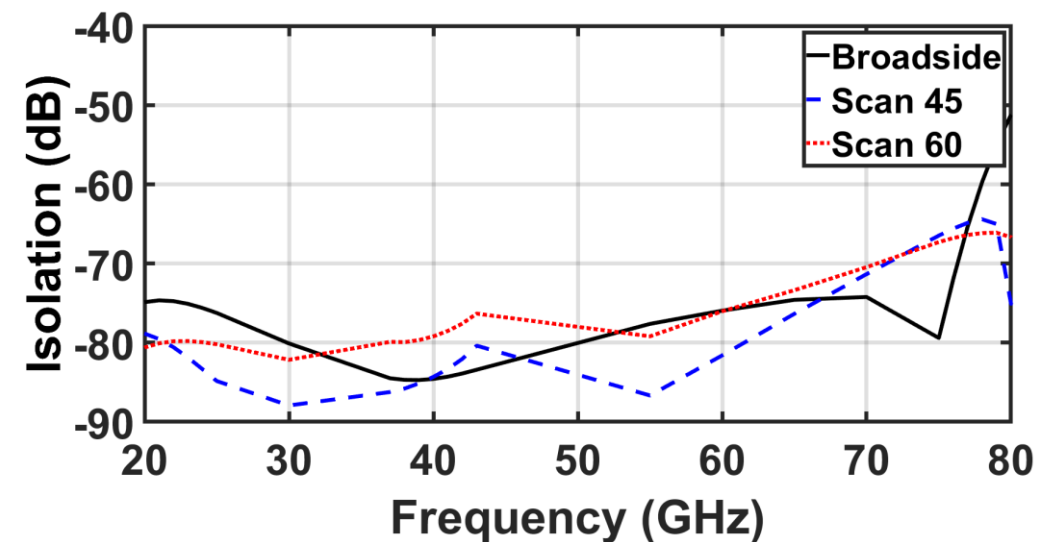
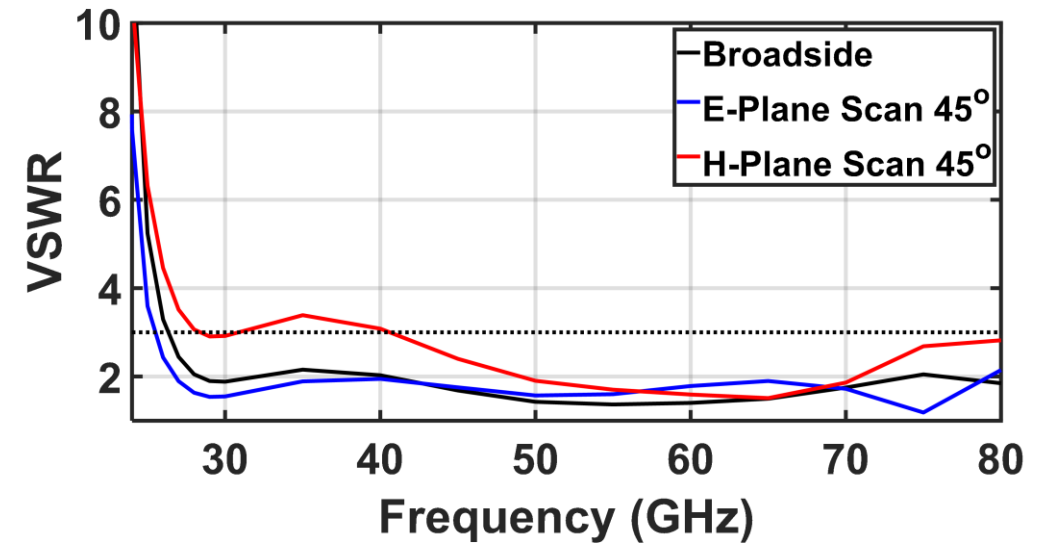
- Implement reflector type high impedance ground plane to minimize phase cancellation.
- Implement high impedance surface as ground plane to kill the surface wave which causes back radiation.
- Using the HIS ground plane the ground height can be reduced.

High Isolation mmWave Antenna for 5G and ISM



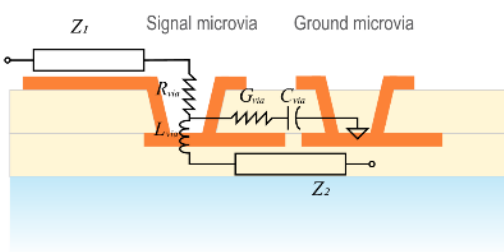
This prototype has:

- A wideband feed
- Dual linear polarization
- VSWR < 3 for 22 GHz to 80 GHz
- Resonance free scanning to 45°
- $H_{\text{Total}} = 1.38\text{mm}$



Interconnects: Fine-Vias for Impedance Matching

LRCG Model



$$R_{via} = \sqrt{R_{via,dc}^2 + R_{via,ac}^2} \quad (1)$$

$$R_{via,dc} = \rho_{cu} \cdot \frac{h}{\pi r^2} \quad (2)$$

$$R_{via,ac} = \frac{p}{2r} \cdot \rho_{cu} \cdot \frac{h}{2\pi r \delta} \quad (3)$$

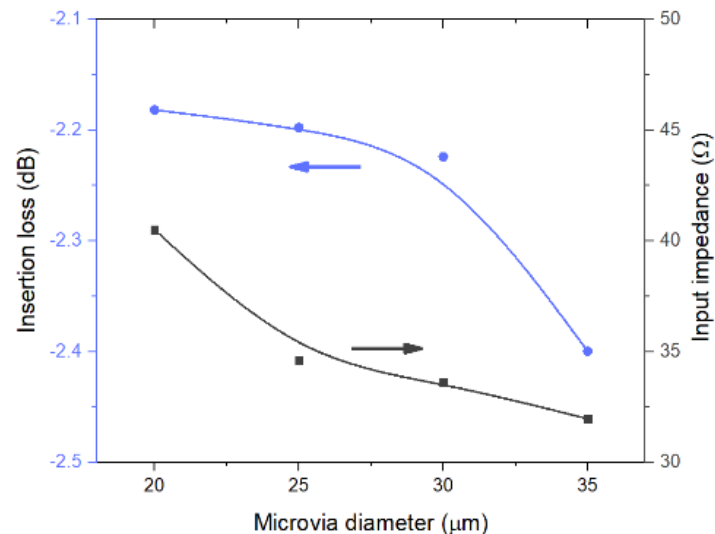
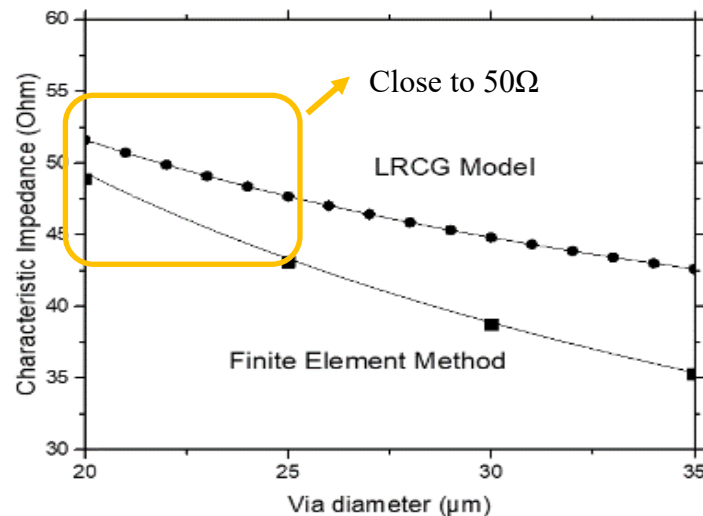
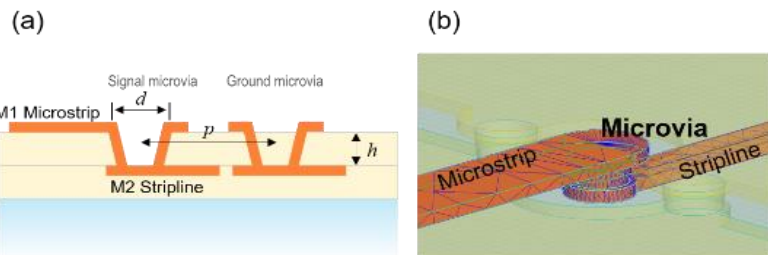
$$L_{via} = \frac{1}{2} \cdot \frac{\mu_{cu}}{2\pi} \cdot h \cdot \ln\left(\frac{p}{r}\right) \quad (4)$$

$$C_{via} = \frac{\pi h \epsilon_r \epsilon_0}{\ln\left(\frac{p}{r}\right)} \quad (5)$$

$$G_{via} = \frac{\sigma_{poly} C_{via}}{\epsilon_r \epsilon_0} \quad (6)$$

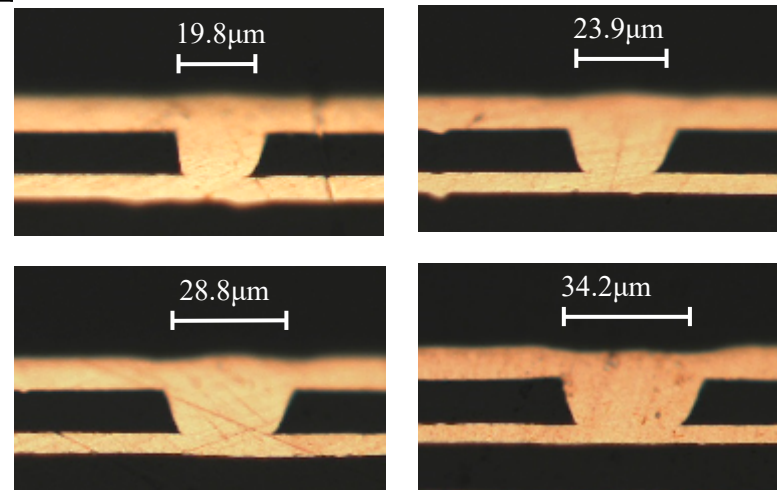
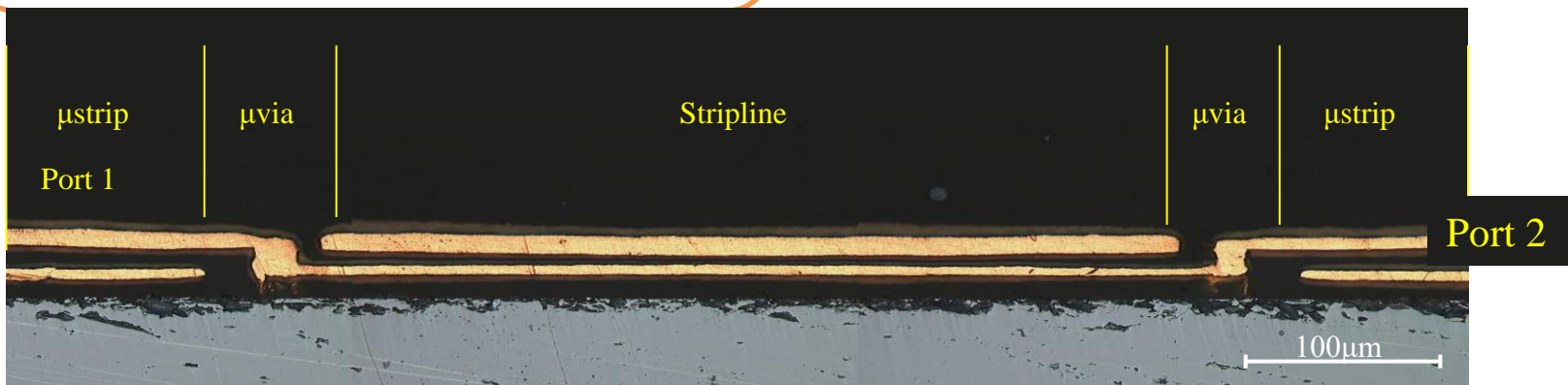
$$Z_{via} = \sqrt{\frac{R_{via} + j\omega L_{via}}{G_{via} + j\omega C_{via}}} \quad (7)$$

FEM Model



(Slide from Atom Watanabe, GT-PRC)

r_{via}	Z_{via}	$20\log(S_{11})$	VSWR	$20\log(S_{21})$
↓	↑	↓ (Less reflection)	↓ (Closer to 1)	↓ (Lower loss)



□ Daisy-chain test vehicle with precise microvia-diameter control to measure microvia losses

High-Performance 5G and LTE Passive Devices

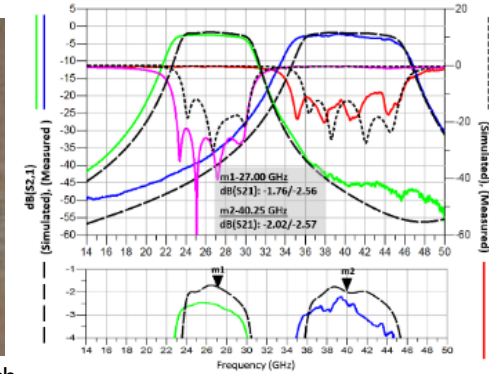
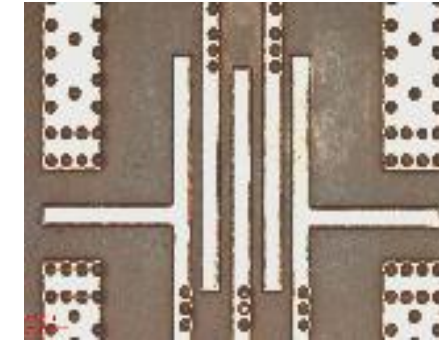
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5G Filters in 50-100 micron glass- or ceramic-core laminates (Muhammad Ali et al., GT-PRC)

- Ultrathin filters: 2X thickness in reduction compared to offchip filters;
- Lower insertion loss compared to on-chip filters

High Q Inductors and LTE Diplexers in glass and glass-core laminates

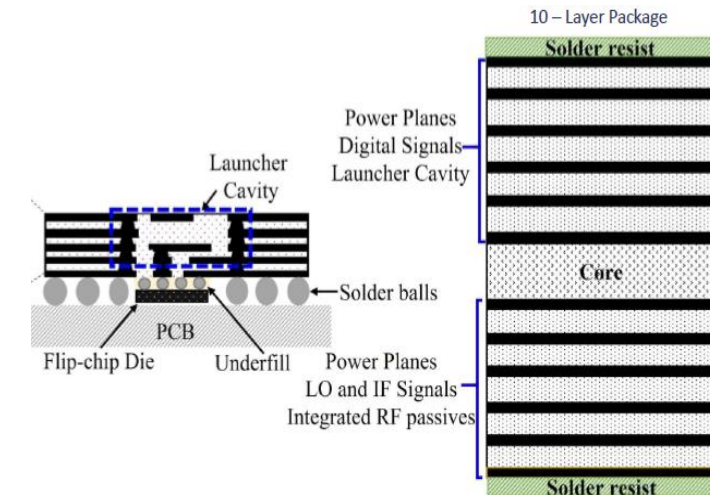
On-Chip	4 dB	0.1 dB/mm	Very Small ($<4\lambda_0^2$)	Very Small ($<500\mu\text{m}$)
Traditional Off-Chip	2 dB	0.5 dB/mm	Small-Med. ($\sim 4\lambda_0^2$)	Med.-Large ($\sim 500\mu\text{m}$)
On-Package – 3D Module	2.5 dB	0.2 dB/mm	Very Small ($<4\lambda_0^2$)	Small ($<500\mu\text{m}$)



- Ultra-fine mm-wave structures with nign precision
- Footprint smaller than 0.5
- Innovative topologies for low insertion loss

Filters in the 100-330 GHz bands (from Neelam Gaunkar et al., Intel)

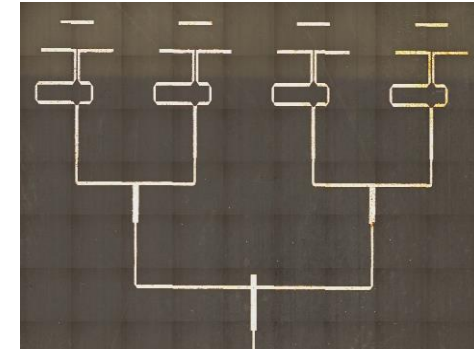
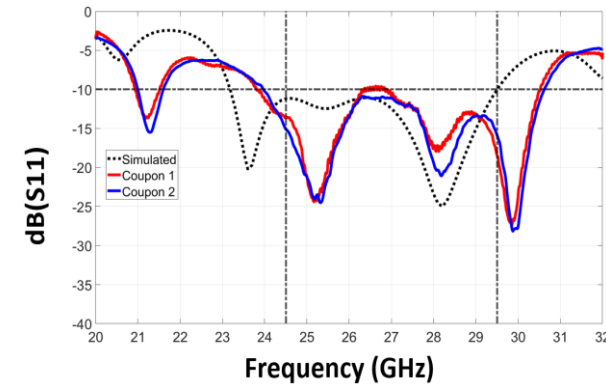
Parameter				
w	10	3.2	2	3
IL (dB)	4-5	3-5	1.7	5-7
Size (mm x mm)	1.9 x 1.35	2 x 0.26	20 x 20 x 40	0.7 – 1.1
Type	Microstrip	Stripline	RWG	SIG
Substrate	Organic	Silicon BCB	Metal	Organic
Operation band	100-140	125-152	200-225	225-330



Power Dividers and Antenna Arrays in Package

Power-dividing networks and High-Gain Antenna Arrays

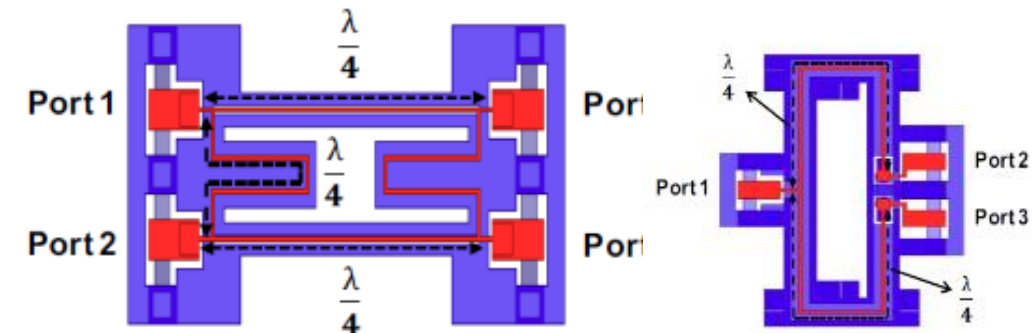
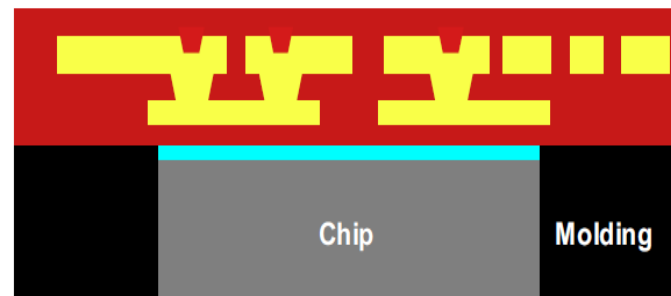
Power Divider and Yagi-Uda Antenna Array	Added Insertion Loss	Realized Gain (27 GHz)	Antenna Array Efficiency
Two-Way, 2×1	0.4 dB	6.96 dBi	80%
Three-Way, 3×1	0.6 dB	8.24 dBi	85%
Four-Way, 4×1	0.86 dB	9.51 dBi	82%



With Atom Watanabe, Muhammad Ali, Tong-Hong Lin, Manos Tentzeris, Rao Tummala et al., (Georgia Tech PRC)

Power-dividing networks and High-Gain Antenna Arrays

InFO (EMC)

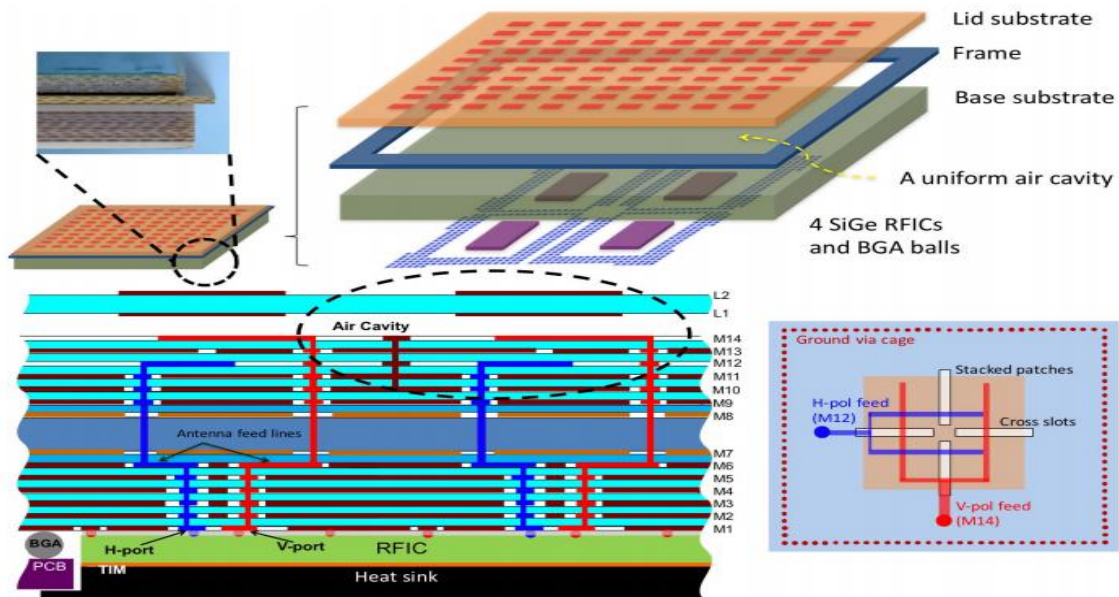


Transmission line insertion loss 0.34 dB/mm
Passive element insertion loss 4.3 – 4.9 dB



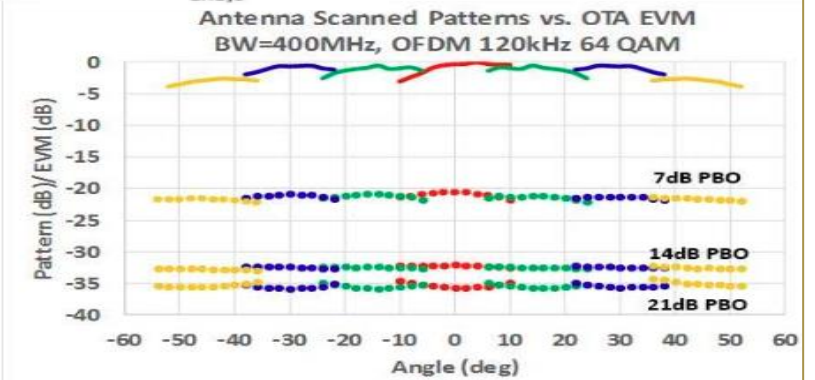
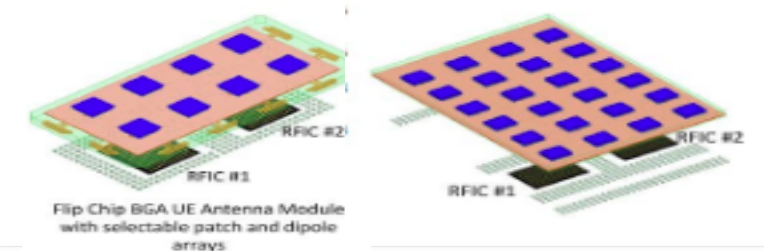
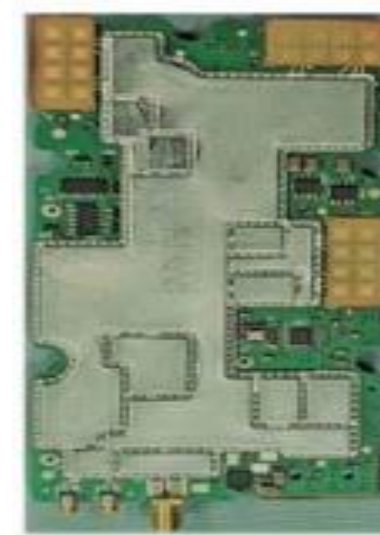
High-Density Packaging: Chip-last mm-wave packages

Organic laminates for Base-station (IBM)



- ✓ High bandwidth because of the air cavity
- ✓ Large-scale antenna array
- ✗ Thick substrate with many metal layers
- ✗ Mechanical reliability

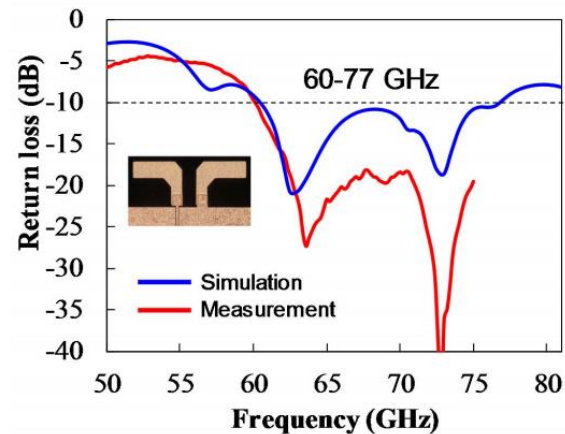
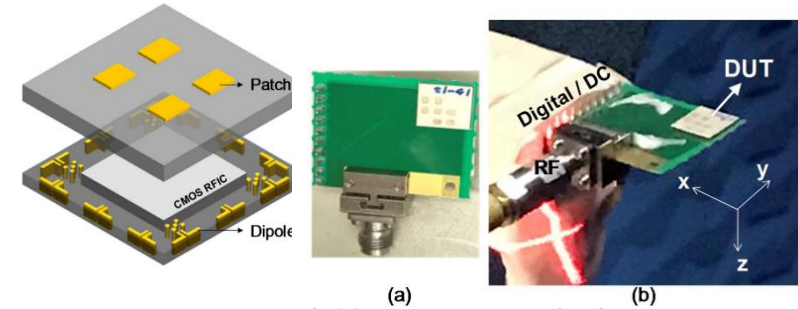
Organic laminates for UE (Qualcomm)



- ✓ Demonstration for handset AiP
- ✓ Co-design from CMOS through AiP
- ✗ Thick substrate with many metal layers

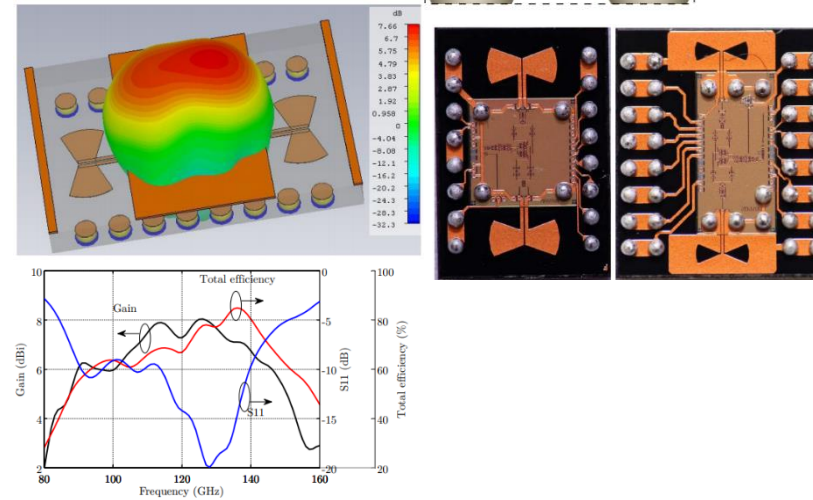
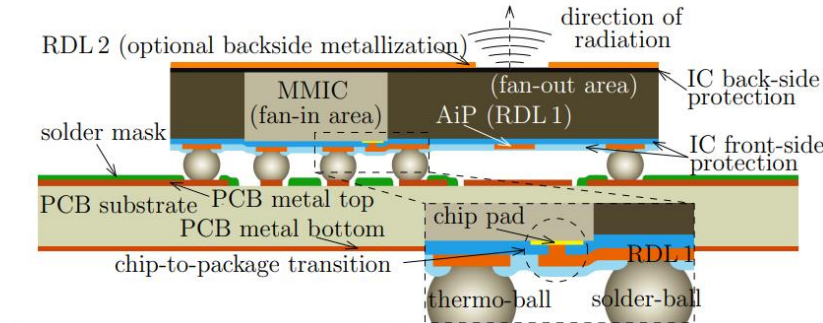
High-Density Packaging: Chip-first mm-wave packages

InFO-AiP (TSMC)



- ✓ Thickness reduction
- ✓ Low signal loss from Chip to Antenna
- × Unbalanced stack-up – Warpage
- × Patterning precision on molding compound

eWLB (Infineon)



- ✓ Thickness reduction
- × Distance variation from Gnd to Patch
- × Patterning precision on molding compound

Fan-out AiP (ASE)

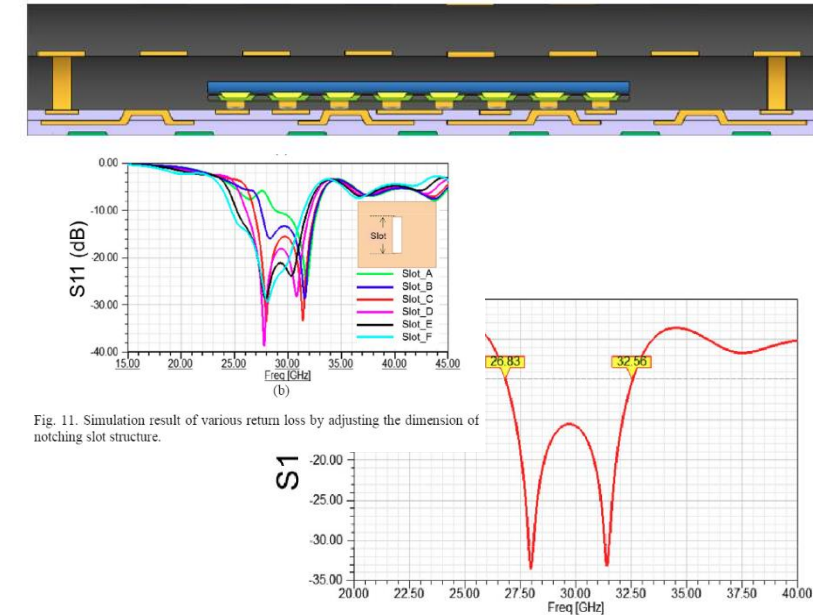


Fig. 11. Simulation result of various return loss by adjusting the dimension of notching slot structure.

Fig. 12. Simulation result of stacking patch antenna

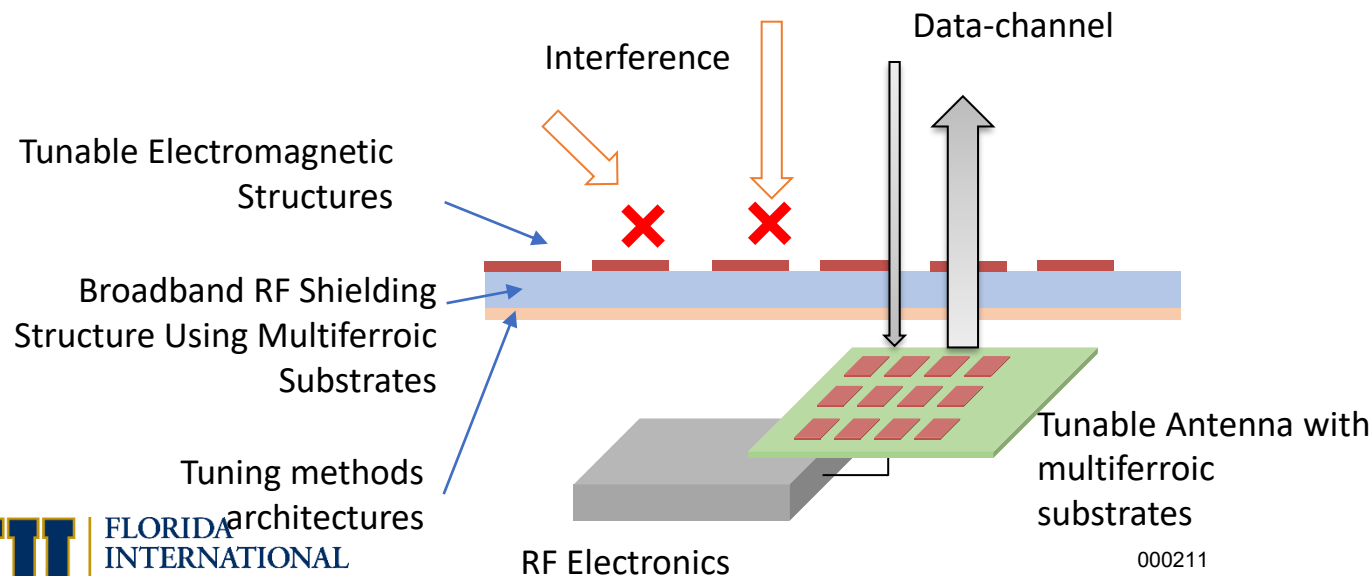
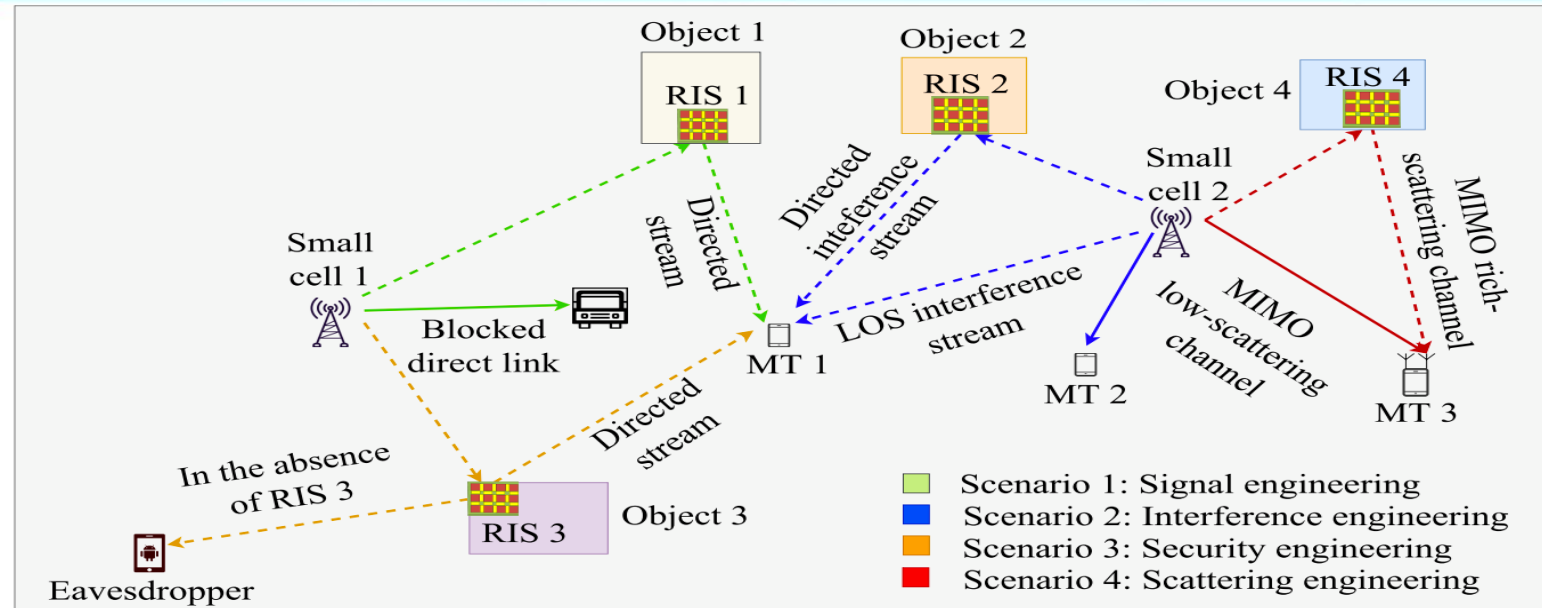
- ✓ Thickness reduction
- × High signal loss in through-mold vias
- × Mold-on-mold causes thickness variations

Tunable or Smart FSS: Selected Examples

Smart Environment with RIS

Need for new materials to achieve:

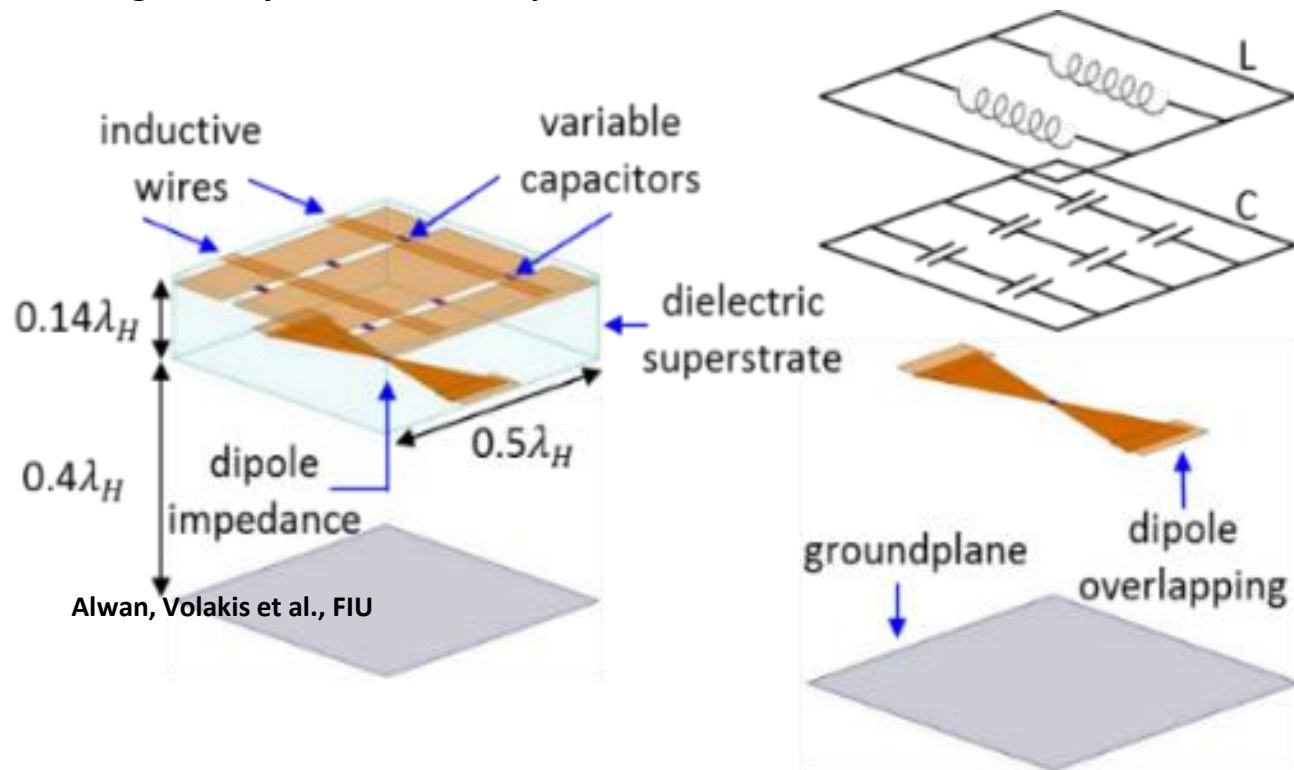
- Security from hacker / eavesdropper;
- Dynamic isolation from a nearby aggressor
- Able to steer the beam with metasurfaces
- Resistive cards to increase gain and bandwidth



- ❑ *Multiferroic based electromagnetic architectures for smart shielding.*
- ❑ *Planar EM substrate architectures for smart substrates (with tunable permittivity) for antennas.*
- ❑ *Frequency selectivity and direction selectivity for EM blocking.*

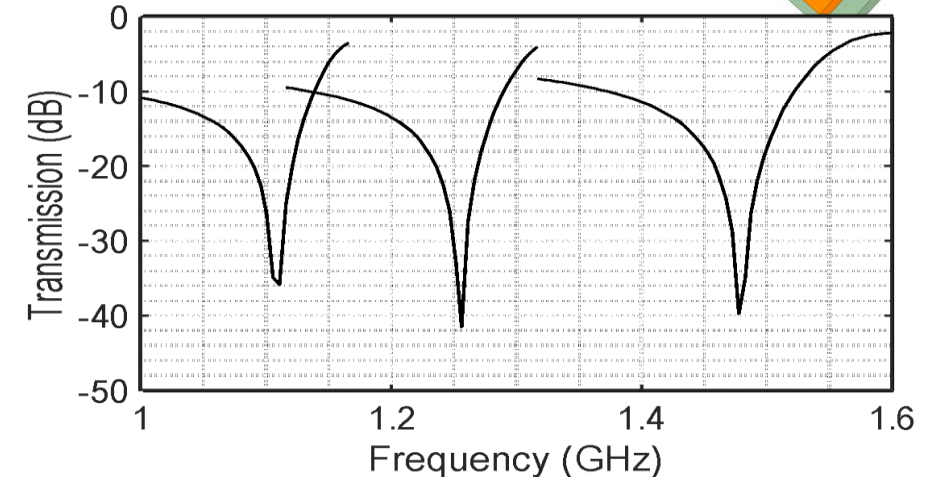
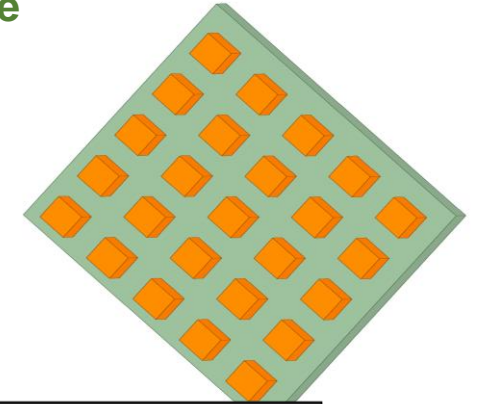
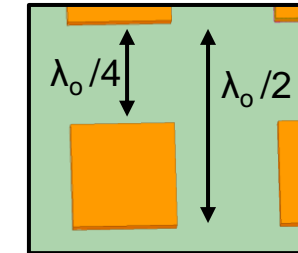
Multiferroic Tunable Shields and Filters for Secure RF Electronics

Reconfigurability with variable capacitors



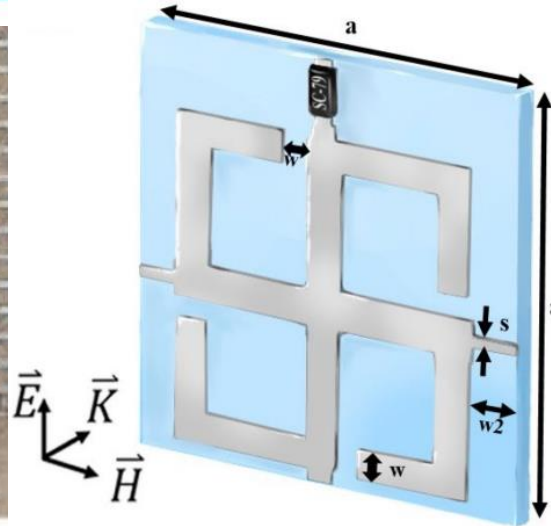
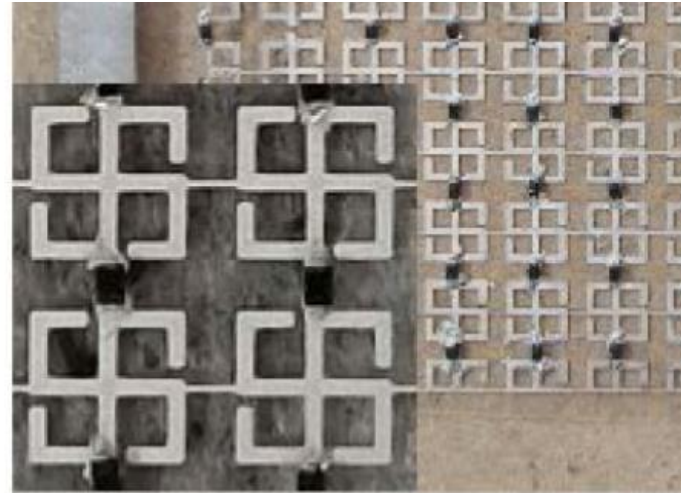
Alwan, Volakis et al., FIU

Variable permittivity substrate Copper

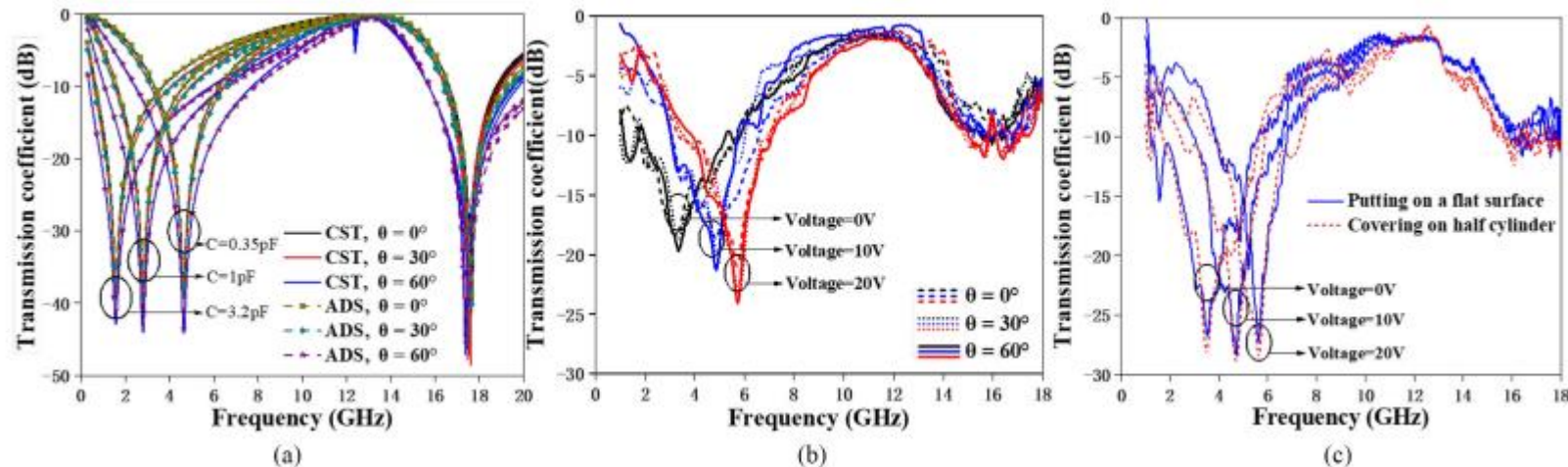


Reconfigurable metasubstrates using multiferroics
Shubhendu Bhardwaj, FIU and UNL :

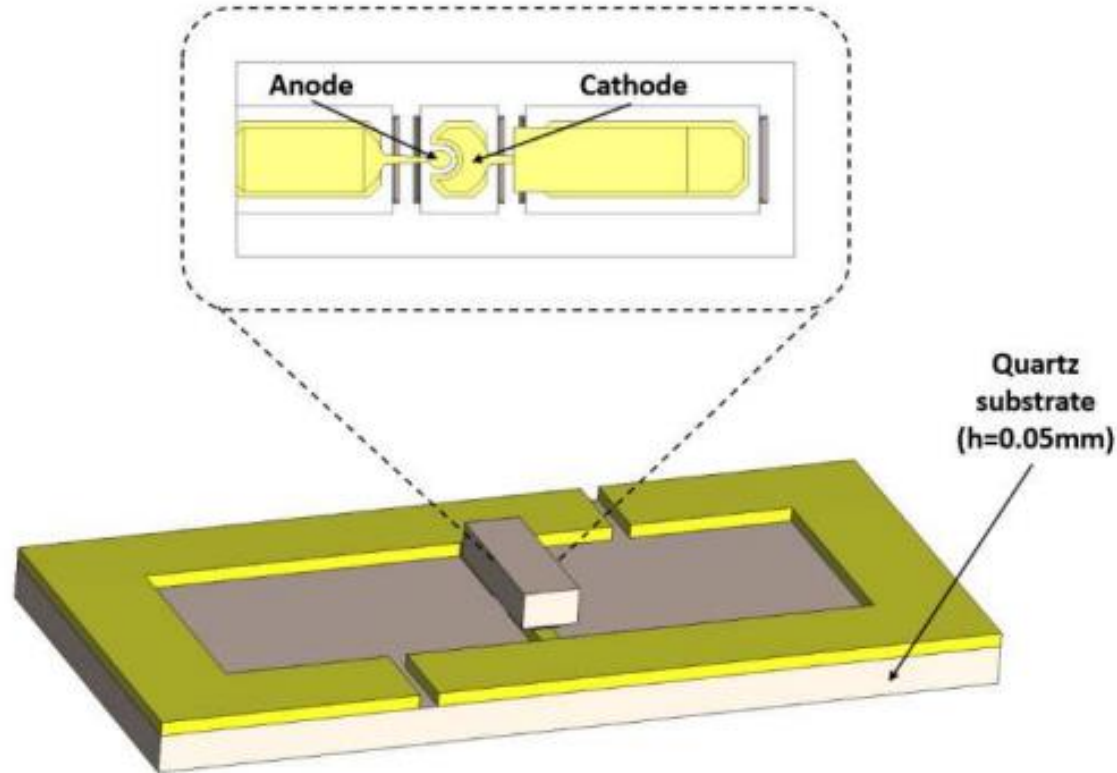
Tunable FSS with PIN Diodes



(a) Simulated transmission coefficient of the FSS varies with the tunable capacitance, under vertical polarized wave. θ is the angle of incident wave. Both CST and ADS are used as a comparison. (b) Measured transmission coefficient under different voltage bias by adjusting the tilted angle of the FSS sample by 0° , 30° , and 60° . (c) Measured transmission coefficient under different voltage bias in cases of putting it on a flat surface and covering on a half cylinder.



Tunable FSS with PIN Diodes



Design of Tunable Millimetre-wave Pass-Band FSS Unit-Cell Loaded with GaAs Air-Bridged Schottky Diodes

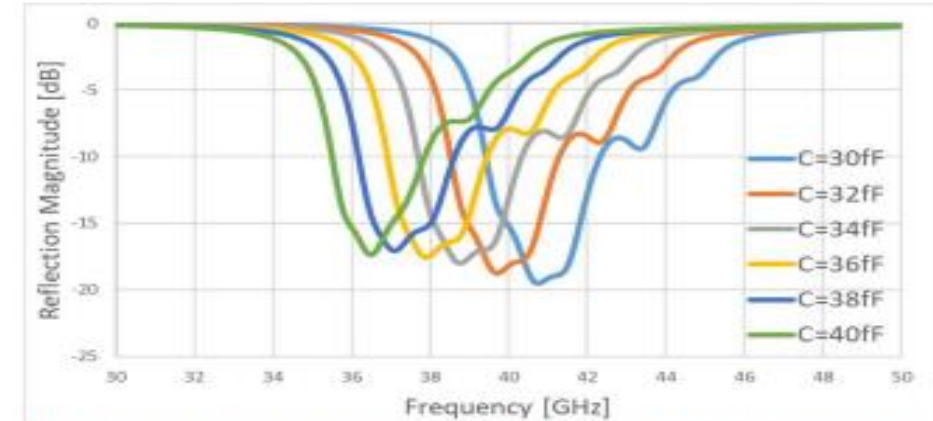


Fig. 8 The magnitude of the reflection coefficient (S_{11}) for the active 5-layer FSS with Schottky diodes mounted and introduce the desired tuning.

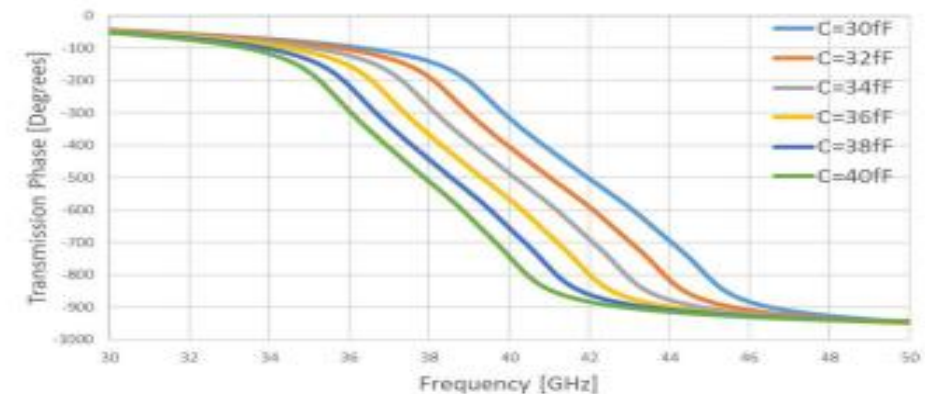
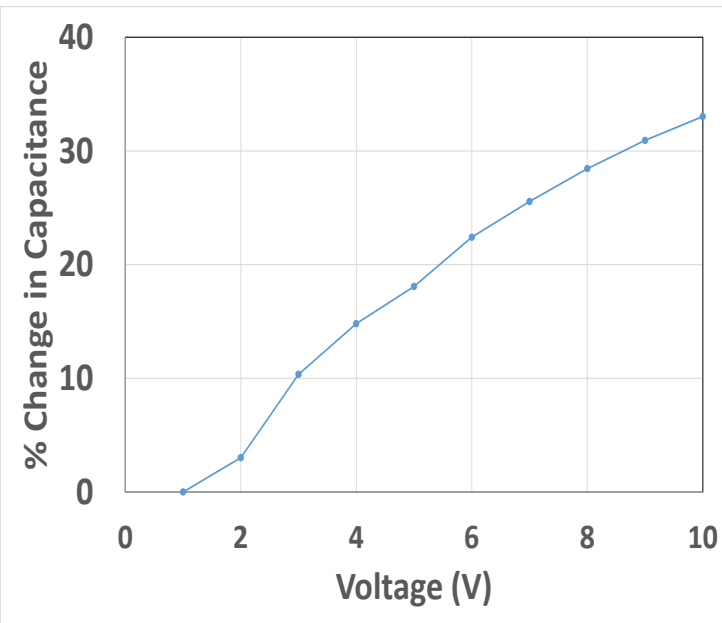


Fig. 9 The phase of the transmission coefficient (S_{21}) for the active 5-layer FSS with Schottky diodes mounted and introduce the desired tuning.

Ioannis Gerafentis, Alexandros Feresidis, Metamaterials Engineering Group,
School of Engineering, University of Birmingham, UK

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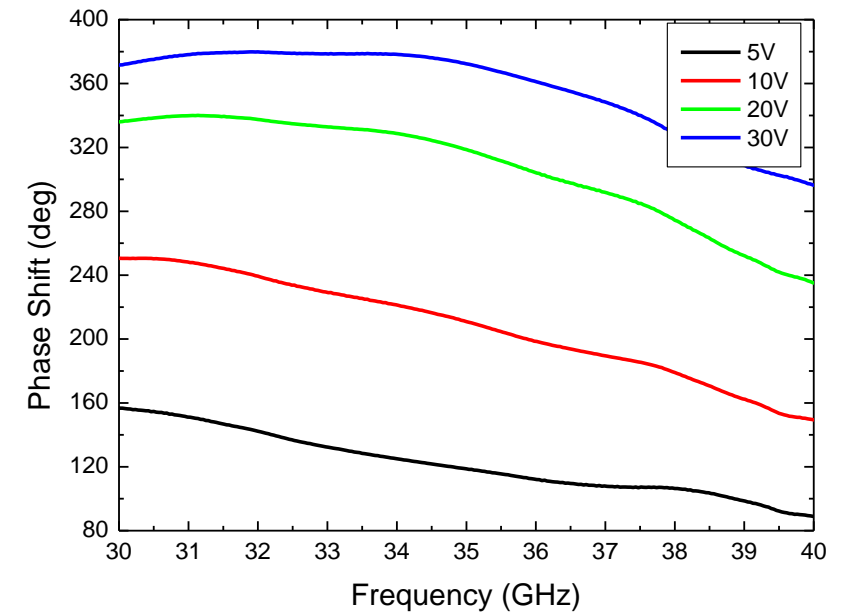
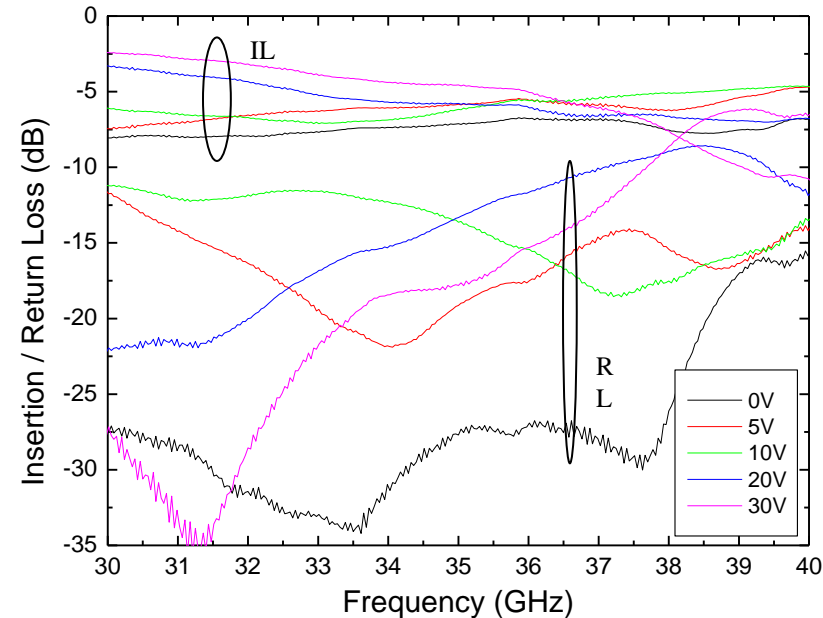
Tunable Ferroelectric Dielectrics



Voltage-based tuning
Need voltages of 5 V/micron

Phase Shifter–Ka-band Typical Performance

Ka-band Phase Shifter



Courtesy of Andrew Hunt, nGimat Co., Norcross, Georgia

Tunable Liquid Crystal Dielectrics

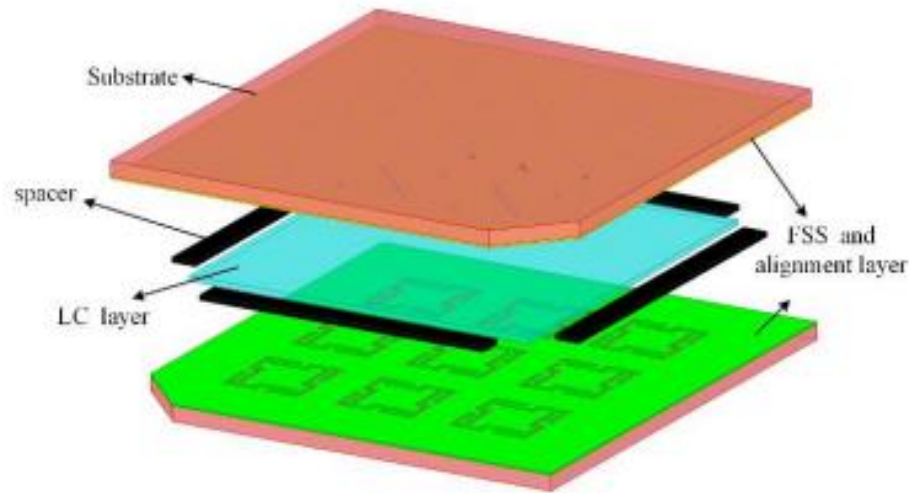


Fig. 1. Architecture of the LC-FSS.

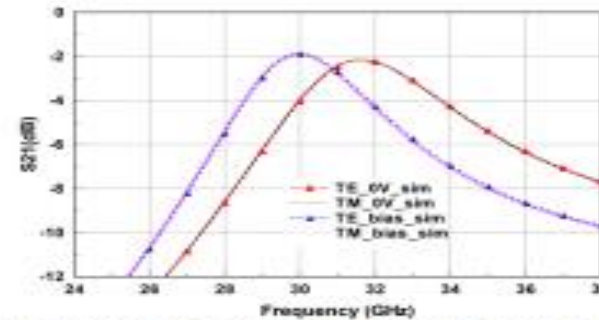
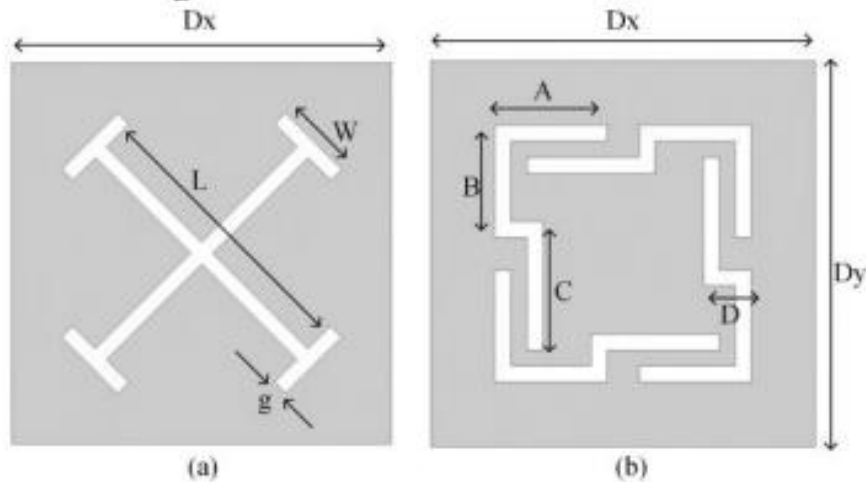


Fig. 3. Comparison of TE and TM polarization for bias and unbiased at normal incident angle.

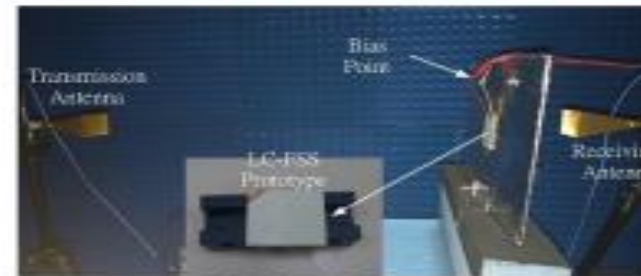


Fig. 4. Setup of measurements

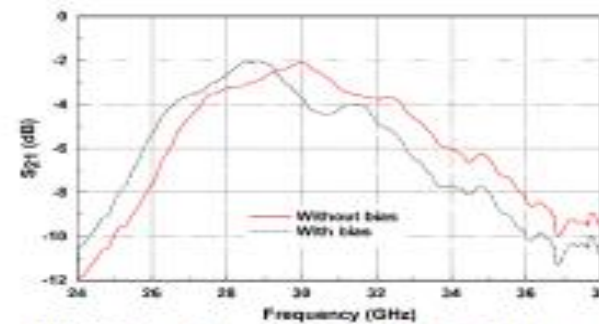
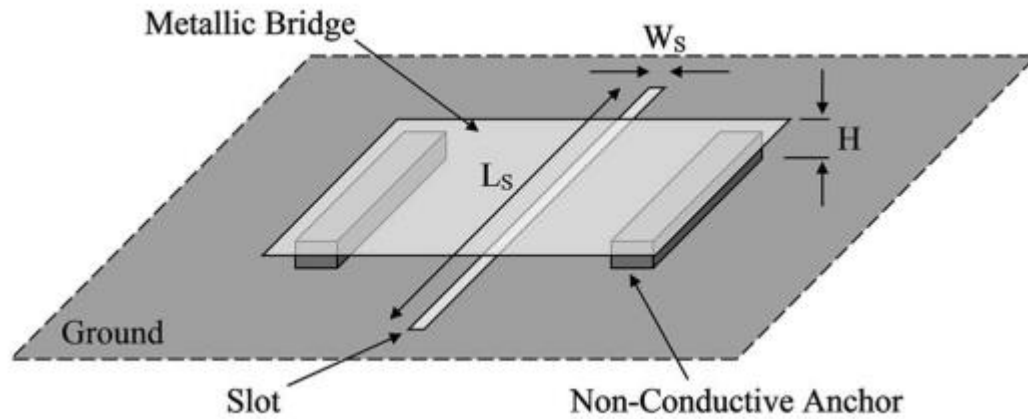


Fig. 5. Transmission response of the LC-FSS prototype with/without bias.

Tunable bandpass liquid crystal frequency selective surface resonating at Ka-band, which has a frequency tunability, closed to 5% of its center frequency.

LC-FSS prototype was fabricated by normal print circuit board (PCB) technology and a Merck-E7 LC material.

MEMS-Based Tunable FSS



Tuning of the resonance frequency is achieved by using a metallic MEMS bridge over the slot. The bridge acts as a capacitive load, increasing the equivalent capacitance, and so decreasing the resonance frequency.

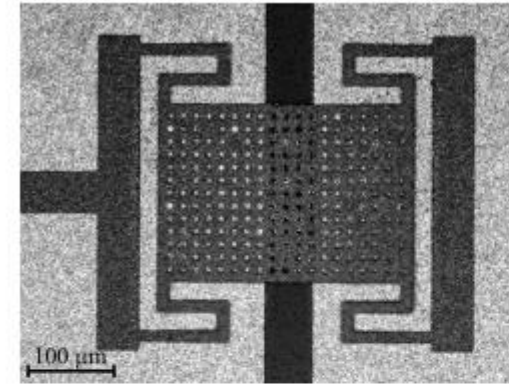


Fig. 9. Picture of the fabricated MEMS bridge.

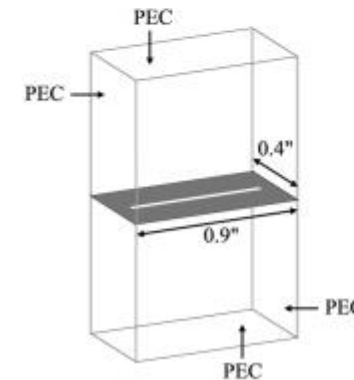


Fig. 10. FSS unit cell simulation setup.

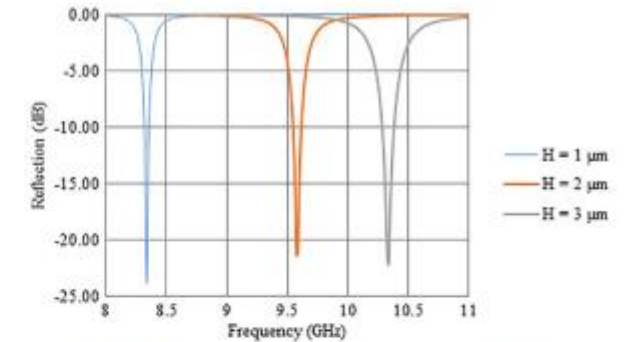


Fig. 11. Simulated response of the FSS unit cell vs. height of the MEMS bridge.

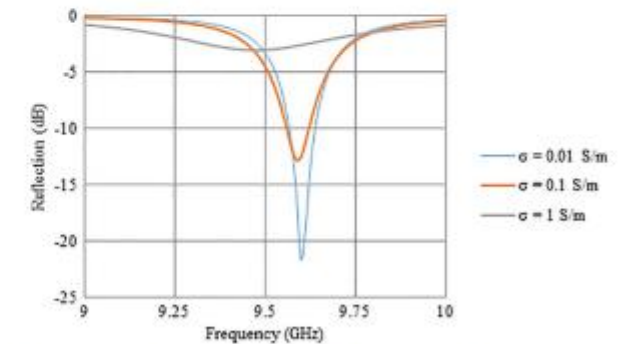


Fig. 12. Simulated response of the FSS unit cell vs. conductivity of silicon anchors 4 μm in height.

X-Band Tunable Frequency Selective Surface Using MEMS Capacitive Loads

Mojtaba Safari, Cyrus Shafai, and Lotfollah Shafai

IEEE TRANSACTIONS ON ANTENNAS AND PROPAGATION, VOL. 63, NO. 3, MARCH 2015

Origami-Based Reconfigurable FSS

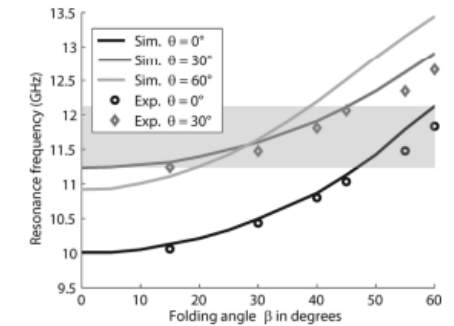
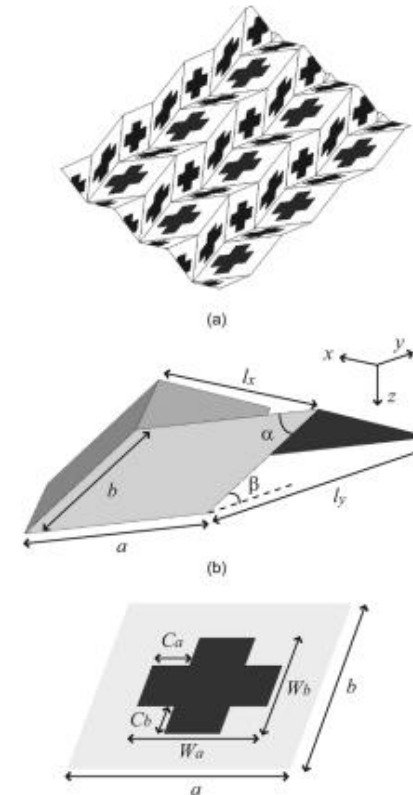
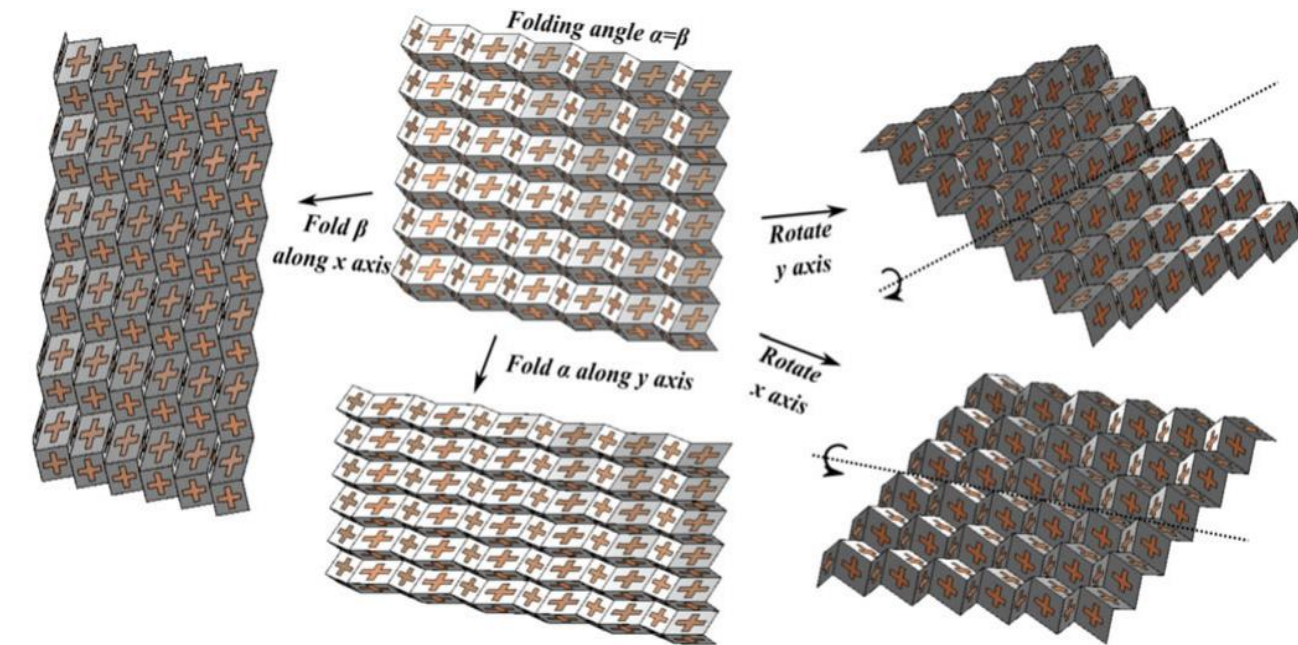


Fig. 3. Simulated and measured resonance frequencies, f_{res} in GHz.

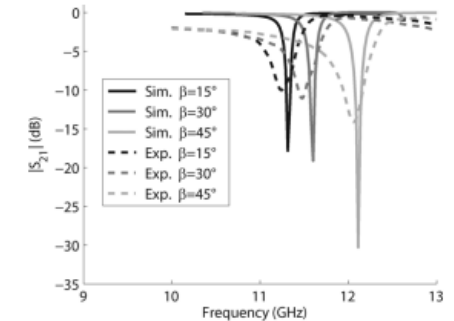


Fig. 4. Simulated and measured transmission coefficient $|S_{21}|$ at oblique incidence at $\theta = 30^\circ$.

A novel 4-DOF wide-range tunable frequency selective surface using an origami “eggbox” structure, Cui, Bahr, Tentzeris

Yepu Cui , Ryan Bahr, Samantha Van Rijs and Manos Tentzeris
International Journal of Microwave and Wireless Technologies

Origami Tunable Frequency Selective Surfaces

IEEE ANTENNAS AND WIRELESS PROPAGATION LETTERS
VOL. 11, 2012

Summary

- **mmWave MIMO with beam-forming (at base stations)** to play a critical role toward 6G
- **RIS** critical for the urban environment: individual phase control
- **In-band full-duplex** is an enabling technology that will play a key role in building 6G
- **UWB antennas** with different antenna designs, coupled with broadband feeding networks
- **Embedded** filters, power dividers, isolation via arrays and solid copper surfaces, impedance-matched interconnects: advanced design rules are needed
- **Tunable FSS** for attaining selective isolation and beamsteering effects